

Assessment of the technological reliability of a hybrid constructed wetland for wastewater treatment in a mountain eco-tourist farm in Poland

Andrzej Jucherski¹, Maria Nastawny¹, Andrzej Walczowski¹,
Krzysztof Józwiakowski² and Magdalena Gajewska³

¹*Mountain Centre of Studies and Implementations in Tylicz, Institute of Technology and Life Sciences in Falenty, Pułaskiego St. 25A, 33-383 Tylicz, POLAND*

²*Department of Environmental Engineering and Geodesy, University of Life Sciences in Lublin, Leszczyńskiego 7, 20-069 Lublin, POLAND (krzysztof.jozwiakowski@up.lublin.pl)*

³*Department of Water and Wastewater Technology, Gdańsk University of Technology, Narutowicza st. 11/12, 80-233, Gdańsk, POLAND*

ABSTRACT

The aim of the present study was to assess the technological reliability of a domestic hybrid wastewater treatment installation consisting of a classic three-chambered (volume 6m³) septic tank, a vertical flow (VF) trickling bed filled with granules of a calcinated clay material (KERAMZYT), a special wetland bed constructed on a slope, and a permeable pond used as a receiver. The test treatment plant was located at a mountain eco-tourist farm on the periphery of the spa municipality of Krynica-Zdrój, Poland. The plant's operational reliability in reducing the concentration of organic matter measured as BOD₅ and COD, was 100% when modelled by both the Weibull and the lognormal distributions. The respective reliability values for total nitrogen removal were 76.8% and 77.0%, total suspended solids – 99.5% and 92.6 %, and PO₄-P – 98.2% and 95.2%, with the differences being negligible. The installation was characterized by a very high level of technological reliability when compared to other solutions of this type. The Weibull method employed for statistical evaluation of technological reliability can also be used for comparison purposes. From the ecological perspective, the facility presented in the study has proven to be an effective tool for protecting local aquifer areas.

Key words: mountain aquifers; rural areas; cold climate; hybrid constructed wetland; technological reliability

INTRODUCTION

Evaluation of the technological reliability of individual wastewater treatment systems should be an important part of planning and decision-making in water and wastewater management, particularly now, when a wide range of technological solutions are available (Józwiakowski et al. 2015). Reliable operation of wastewater treatment units must be ensured due to both environmental and human health protection concerns (Eisenberg et al. 2001; Wojciechowska et al 2016). Reliable operation of domestic wastewater treatment plants is especially important in mountain aquifer areas, which are very sensitive to pollution. Mountainous regions in Poland play a key role in developing and sustaining vital socio-economical and environmental functions which intertwine in the activities of spa and tourist resorts, forest management, environment-friendly farming and especially in hydrology.

1 Although Polish mountainous areas have a high water production potential, as manifested by
2 an almost 40% regional surplus in relation to the water discharged by all the rivers, Poland
3 occupies one of the last positions in Europe in terms of the total freshwater resources, which
4 are estimated at 1630 m³·year⁻¹·person⁻¹. Therefore, it is essential that groundwater and the
5 upper reaches of local streams and mountain rivers should be protected against biological,
6 chemical and bacteriological pollution resulting from the discharge of untreated domestic
7 sewage to the environment in rural areas. One of the key issues in technological progress in
8 wastewater management in rural, environmentally valuable areas, is the construction of small
9 domestic or local wastewater treatment plants with a high, long-term reliability and
10 effectiveness in reducing wastewater pollutions (Jucherski & Walczowski 2012; Masi et al.
11 2013; Józwiakowski et al. 2016; Gajewska et al. 2015).

12 Nowadays, more and more innovative wastewater treatment systems are being designed
13 and offered on the market, which spurs the need for developing a universal method of
14 assessing the reliability of the various treatment processes and facilities. Such a method would
15 be helpful in planning and comparing the levels of protection offered by the various
16 technologies (Józwiakowski et al. 2015).

17 The methods for determining the reliability of individual wastewater treatment systems
18 have been described in more detail by Eisenberg et al. (2001). Lately Djeddou & Achour
19 (2015) have proposed a method for predicting reliability using artificial neural networks.

20 A comprehensive and useful assessment of the reliability of domestic wastewater
21 treatment plants should be based on a series of measurements and observations of treatment
22 variability under normal and critical operating conditions as well as the probability of
23 mechanical failures and their impact on the quality of the treated wastewater (Eisenberg et al.
24 2001).

25 Reliability is defined as the probability of achieving required performance of a wastewater
26 treatment plant (WWTP) over a specific time and under specific conditions (Oliveira &
27 Sterling 2008). To assess WWTP, a coefficient of reliability (CR) which relates mean
28 pollutant concentrations to effluent standards (Niku et al. 1982) can also be used.

29 The statistical step in the assessment of WWTP reliability presented in this article is based
30 on the normal (Niku et al. 1982), the lognormal (Oliveira & Sterling 2008) and the Weibull
31 distributions (Bugajski et al. 2012; Nastawny & Jucherski 2013; Wałęga 2009). Statistical
32 distributions of probability are used to establish the probability of occurrence of selected
33 values of pollutants. Recent findings reported in the literature (Bugajski et al. 2012; Bugajski

2014; Nastawny & Jucherski 2013; Wałęga 2009) show that the Weibull distribution is an accurate and precise tool for evaluation of WWTP reliability.

Systems for domestic wastewater management are individual facilities with technical and quasi-technical treatment devices designed to collect and treat wastewater to the extent required by specific regulations (Regulation of the Polish Minister of Environment 2014) as well as discharge it to receivers without adversely affecting the soil–water complex in the place where the facilities are located. In rural areas, individual treatment facilities usually operate without constant supervision and are therefore particularly exposed to fluctuations in efficiency due to a variable load pattern (Massoud et al. 2009; Platzer & Mauch 1997); in consequence, the quality of effluent often does not meet the requirements stipulated in the regulations in force.

Hybrid wetland systems have recently been more and more frequently used for the treatment of domestic wastewater from museum buildings and forester or mountain shelters, including those located in national parks. When well designed and properly maintained, they can achieve high pollutant removal efficiencies (Masi et al. 2007; Osaliya et al. 2011; Józwiakowski et al. 2014; Sanchez-Ramos et al. 2015; Gizińska-Górna et al. 2016; Józwiakowski et al. 2016). The literature, however, provides little data on the reliability of pollutant removal processes in such CWS over long periods (years) of operation.

The aim of the present study was to assess the range of long-term fluctuations in treatment reliability in a domestic hybrid wastewater treatment plant. The plant had been built over ten years before on an eco-tourist farm in the mountain municipality and spa of Krynica-Zdrój in Poland and had been continuously operating since that time. The following indicators of wastewater contamination were measured: (i) BOD₅ and COD for contamination with organic matter, (ii) total suspended solids, (iii) total nitrogen (TN), and (iv) phosphorus PO₄-P. The indicators results (pollutant concentrations) were compared to the Polish standards for treated wastewater (Regulation of the Polish Minister of Environment 2014) discharged into water and soil from treatment plants below 2000 PE.

MATERIAL AND METHODS

The subject of the study was a hybrid wastewater treatment plant described in detail by Jucherski & Walczowski (2012). The plant was operated by an eco-tourist farm located in the rural peripheries of the spa town of Krynica-Zdrój, Poland. The plant had been monitored over the years 2005–2015. A schematic of the facility with the sampling points is presented in Fig. 1.

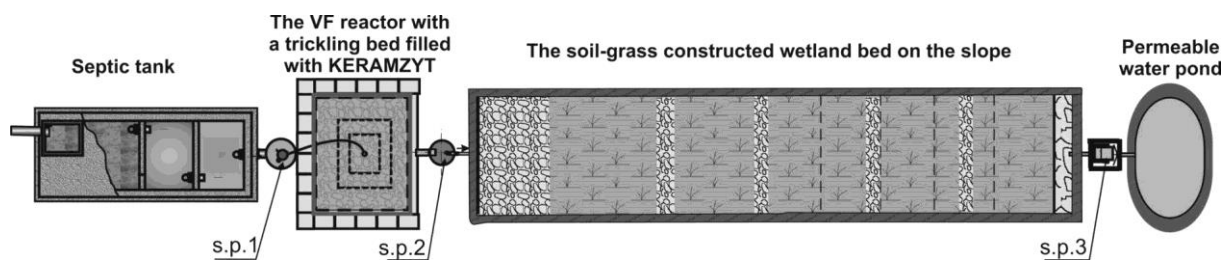


Figure 1. Schematic of the wastewater treatment installation (sampling points: s.p.1, s.p.2, s.p.3)

The installation consisted of a classic three-chamber septic tank, a vertical flow reactor (filter) followed by a special constructed wetland (SCW), and a permeable water pond as a receiver of the final effluent. The septic tank, with a capacity of 6m^3 , was a monolithic concrete structure designed to receive sewage with a seasonal variability from 3 to 15 persons (with an average of $\text{PE}=5$). The substrate used in the vertical flow reactor were granules of a sintered clay material (KERAMZYT). To improve biological treatment and nitrification at the vertical stage, the wastewater was sprayed onto the surface of the reactor. Due to the harsh climate, it was necessary to use a cover to insulate the reactor from freezing in winter. Downstream of the reactor, there was a special filter bed (wetland) with subsurface flow, planted with a mix of reed sweet grass (*Glyceria maxima*), reed canary grass (*Phalaris arundinacea*) and other grasses spontaneously inhabiting the bed. The bed was constructed on a slope for tertiary treatment and removal of the remaining nutrients (N and P). The installation ended with a permeable pond for receiving and infiltration of the treated wastewater into the soil complex surrounding the treatment unit.

The average hydraulic load of the treatment plant in the investigation period was $621.2\text{ dm}^3\cdot\text{day}^{-1}$, and the average concentrations of pollutants in raw sewage were $271.7\text{ mg O}_2\cdot\text{dm}^{-3}$ for BOD_5 , $390.8\text{ mg O}_2\cdot\text{dm}^{-3}$ for COD, $75.4\text{ mg}\cdot\text{dm}^{-3}$ for total suspended solids, $110.5\text{ mg}\cdot\text{dm}^{-3}$ for total nitrogen, and $12.3\text{ mg}\cdot\text{dm}^{-3}$ for phosphorus $\text{PO}_4\text{-P}$ (Table 1). The flow of treated wastewater was calculated based on the water consumption reading of a water meter. BOD_5 was determined using the OxiTop respirometric measuring system from WTW. COD, total nitrogen and phosphate phosphorus were determined using a Merck SQ118 photometer and a Merck thermoreactor TR-200. The total suspended solids were determined by a gravimetric method, in accordance with the standard PN-72/C-04559/02.

The statistical analysis was based on the normal, lognormal and Weibull distributions. Statistica v. 13.0 software was employed to define the characteristics of the distribution of the empirical data using the Kolmogorov-Smirnov goodness-of-fit test. Data were tested for

normality of distribution by measuring the distance between the empirical distribution and the theoretical distribution. The following null hypothesis was tested at 0.05 level of significance: distribution of the variable is normal/lognormal/Weibull. Furthermore the quality of fit of the Weibull distribution to empirical data was assessed using the Hollander–Proschan test for the significance level of 0.05. The reliability function $R(x)$ was calculated as a complement to the cumulative distribution function using the following formula:

$$R(x) = 1 - F(x) \quad [1]$$

where x is an indicator of the concentration of pollutants in treated wastewater (Bugajski et al. 2012).

Reliability was determined from cumulative distribution plots, taking into consideration pollutant concentrations in treated wastewater permitted by the Regulation of the Polish Minister of Environment (2014), i.e.: $BOD_5 \leq 40 \text{ mg O}_2 \cdot \text{dm}^{-3}$, $COD \leq 150 \text{ mg O}_2 \cdot \text{dm}^{-3}$, total suspended solids $\leq 50 \text{ mg} \cdot \text{dm}^{-3}$, total nitrogen $\leq 30 \text{ mg} \cdot \text{dm}^{-3}$, total phosphorus $\leq 5 \text{ mg} \cdot \text{dm}^{-3}$.

RESULTS AND DISCUSSION

The many-year means of effluent contaminant concentrations in wastewater treated in the investigated installation ($BOD_5 - 3.49 \text{ mgO}_2 \cdot \text{dm}^{-3}$, $COD - 28.0 \text{ mgO}_2 \cdot \text{dm}^{-3}$, suspended solids $- 15.8 \text{ mg} \cdot \text{dm}^{-3}$, total nitrogen $- 20.9 \text{ mg} \cdot \text{dm}^{-3}$, and phosphorus $P-PO_4 - 1.70 \text{ mg} \cdot \text{dm}^{-3}$) (Table 1) were much lower than required by the Regulation (2014) on discharging wastewater into the soil or surface waters including lakes and their tributaries, and artificial water reservoirs situated on flowing waters.

Table 1 shows the basic statistics for pollutant concentration in wastewater.

Table 1. Basic statistics for pollutant concentrations in wastewater

Parameter		Number of samples	Mean	Median	Minimum	Maximum	Standard deviation	Coefficient of variation
			$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	%
BOD_5	inlet	57	271.7	230	90	580	132.9	48.8
	outlet	49	3.49	2.5	0	13	2.92	83.6
COD	inlet	61	391	353	214	641	114.9	29.4
	outlet	55	28	25	5	112	17.6	63
Suspended solids	inlet	48	75.4	66	19	218.6	40.5	53.7
	outlet	41	15.8	14	0	44.6	10.9	69.2
Total nitrogen N_{tot}	inlet	61	110.5	105.5	70.3	193.8	19.5	17.6
	outlet	55	20.9	19.5	1.6	64.8	16.4	78.5
Phosphorus $PO_4\text{-P}$	inlet	65	12.3	11.1	7.6	24.9	3.97	32.3
	outlet	59	1.7	1.5	0.14	5.46	1.23	72.2

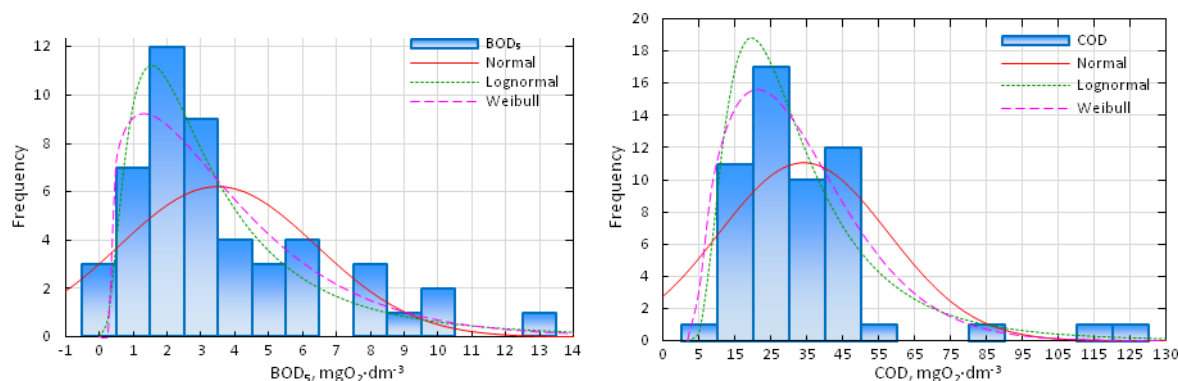
The effluent quality indicators were characterized by high coefficients of variation (Table 1) which, though statistically significant (and therefore useful for the evaluation of the treatment processes in the installation), were too low to have any relevance from the point of view of environmental protection. To determine the technological reliability of the treatment plant, a detailed statistical analysis was performed based on the distributions of the empirical data of each effluent contaminant. The normal, lognormal and Weibull distributions (Table 2, Fig. 2) were adjusted to data sets obtained during the 10-year study.

Table 2. The Kolmogorov-Smirnov goodness-of-fit statistics and significance levels for the analyzed empirical distributions

Distribution	Normal		Lognormal		Weibull	
	stat	p	stat	p	stat	p
BOD ₅	0.2076	0.0324	0.1118	0.5751	0.1354	0.3371
COD	0.1388	0.2183	0.0970	0.6427	0.1157	0.4208
TSS	0.0944	0.8454	0.1416	0.3786	0.1067	0.7262
Total nitrogen N _{tot}	0.1422	0.1960	0.1604	0.1056	0.1085	0.5028
Phosphorus PO ₄ -P	0.1093	0.4501	0.0926	0.6585	0.0507	0.9962

Symbols: stat – value of the statistic test, p – significance level of the test; when p is greater than 0.05, the distribution of empirical data can be described by the analyzed distribution

Statistical analysis using the Kolmogorov-Smirnov goodness-of-fit test showed that the Weibull and lognormal distributions could be well fitted to the empirical distributions of each pollution indicator, whereas the normal distribution gave a much worse fit, although it could also be used for most of the parameters, except BOD₅ (Table 2).



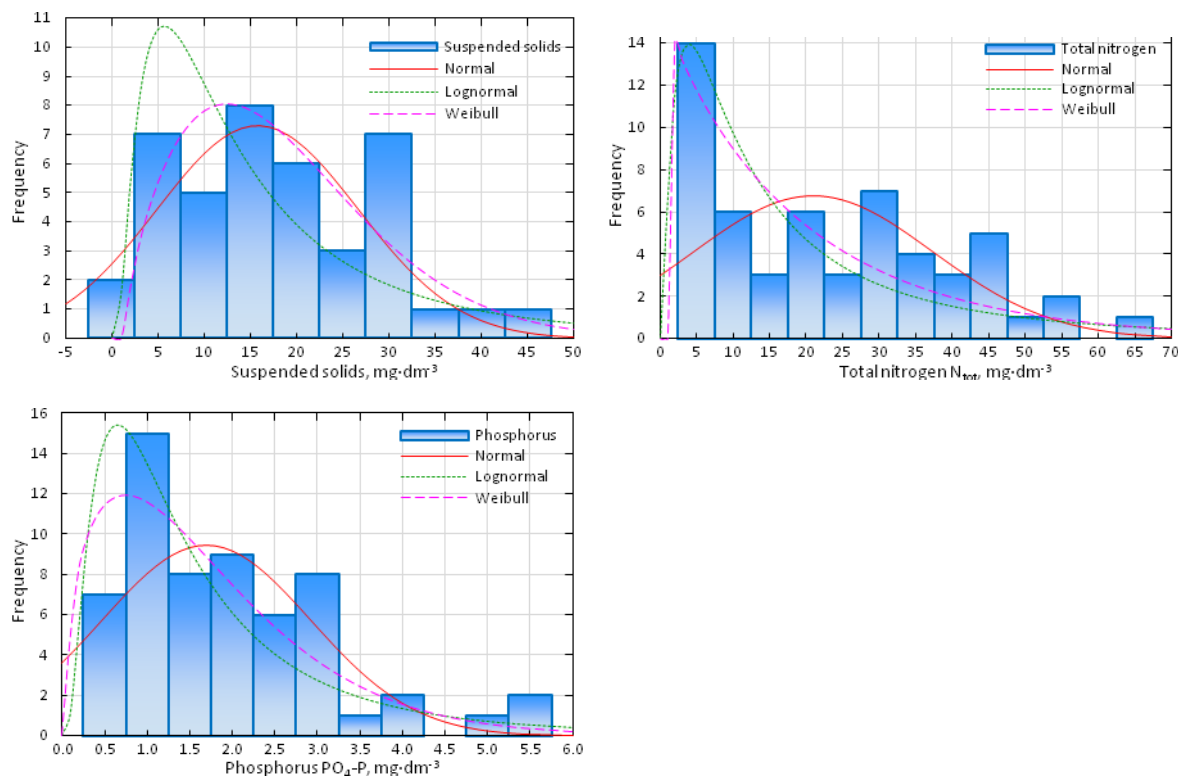


Figure 2. Histograms of the normal, lognormal and Weibull distributions of the empirical data

Based on the detailed analysis and evaluation of the WWTP, as reported above, its reliability was modelled using the Weibull distribution (Table 3, Fig. 3). This allowed us to compare our results with those obtained by other authors (Bugajski et al. 2012; Nastawny & Jucherski 2013; Wałęga 2009) who had used the same distribution. In addition, the indicators of the technological reliability of the treatment plant were also compared to values obtained from the lognormal distribution. The parameters of the Weibull distribution were calculated using the maximum likelihood estimation. In order to determine the goodness of fit of the Weibull distribution to the empirical data described by the distribution parameters (Table 3), the Hollander–Proschan test was applied. As can be seen from Table 3, the goodness of fit of the obtained distributions was high and ranged from 72 to 98% at a significance level of 0.05 (Table 3).

Table 3. Parameters of the Weibull distribution and the Hollander–Proschan goodness-of-fit test

Parameter	Parameters of Weibull distribution			Hollander–Proschan goodness-of-fit test	
	Location	Shape	Scale	stat	p
BOD ₅	0.3182	1.2479	3.6602	0.2150	0.8297
COD	2.4697	1.5798	28.5112	0.0200	0.9840
Suspended solids	-0.6212	1.6638	19.2133	-0.1235	0.9017
Total nitrogen N _{tot}	1.2364	0.9844	19.5929	-0.3558	0.7220
Phosphorus PO ₄ -P	0.0707	1.3664	1.7796	0.0411	0.9672

Symbols: stat - value of the statistic test, p - significance level of the test; when $p \leq 0.05$ the distribution of data is not Weibull distribution

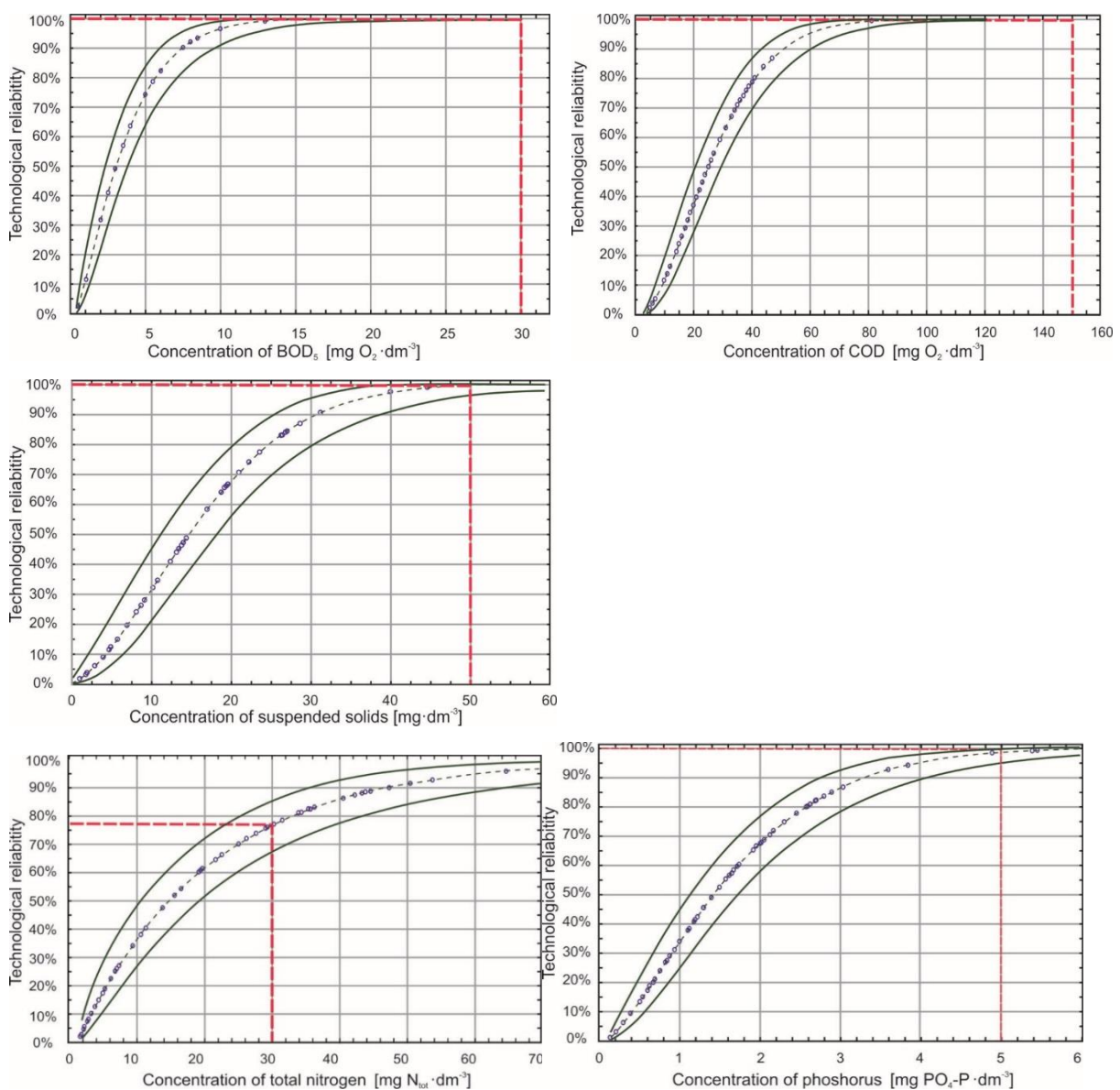


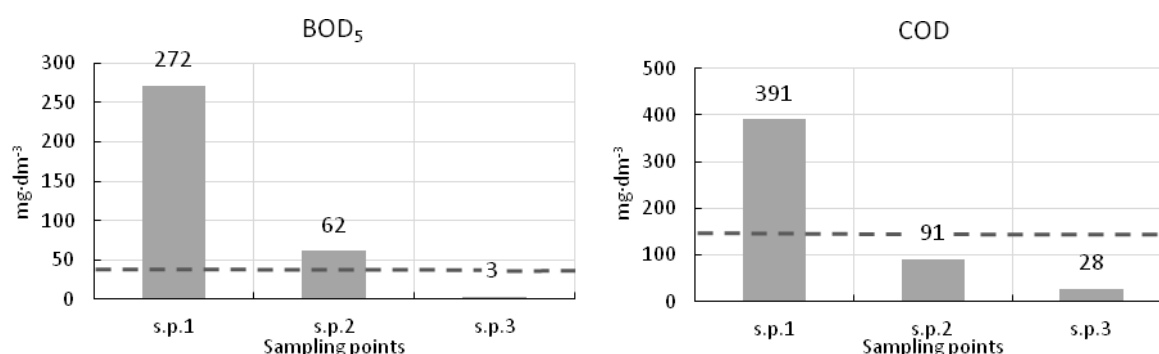
Figure 3. Weibull cumulative distribution functions and the technological reliabilities determined for each pollution parameter with estimated confidence intervals of 95.0%

The technological reliabilities of the installation determined by the Weibull distribution function compared to the lognormal distribution are given in Table 4. It was shown that the reliability of reducing BOD₅ and COD concentrations was 100% both for the lognormal as well as the Weibull distribution functions. For other pollutants, the reliabilities of the treatment plant described by the lognormal distribution and the Weibull distribution were slightly lower at 92.6% and 99.5% for TSS, 77.0% and 76.8% for N_{tot}, and 95.2% and 98.2% for phosphorus PO₄-P, respectively (Fig. 3, Table 4).

Table 4. The technological reliability of the facility for wastewater treatment [in %] determined using the Weibull and the lognormal distribution functions

Parameter	Weibull distribution	Lognormal distribution
BOD ₅	100	100
COD	100	100
Suspended solids	99.5	92.6
Total nitrogen N _{tot}	76.8	77.0
Phosphorus PO ₄ -P	98.2	95.2

The results of this study demonstrate that the wastewater treatment processes were stable and reliable as well as very effective. As shown by the graphs in Figure 4 and the Helsinki Commission Recommendation (HELCOM 2007) data in Table 5, the average values of the parameters of the treated wastewater met the Polish requirements (Regulation of the Polish Minister of Environment 2014). Therefore, treated wastewater could be discharged into the environment throughout the year, with soil receiver sites being preferred over other receiver bodies.



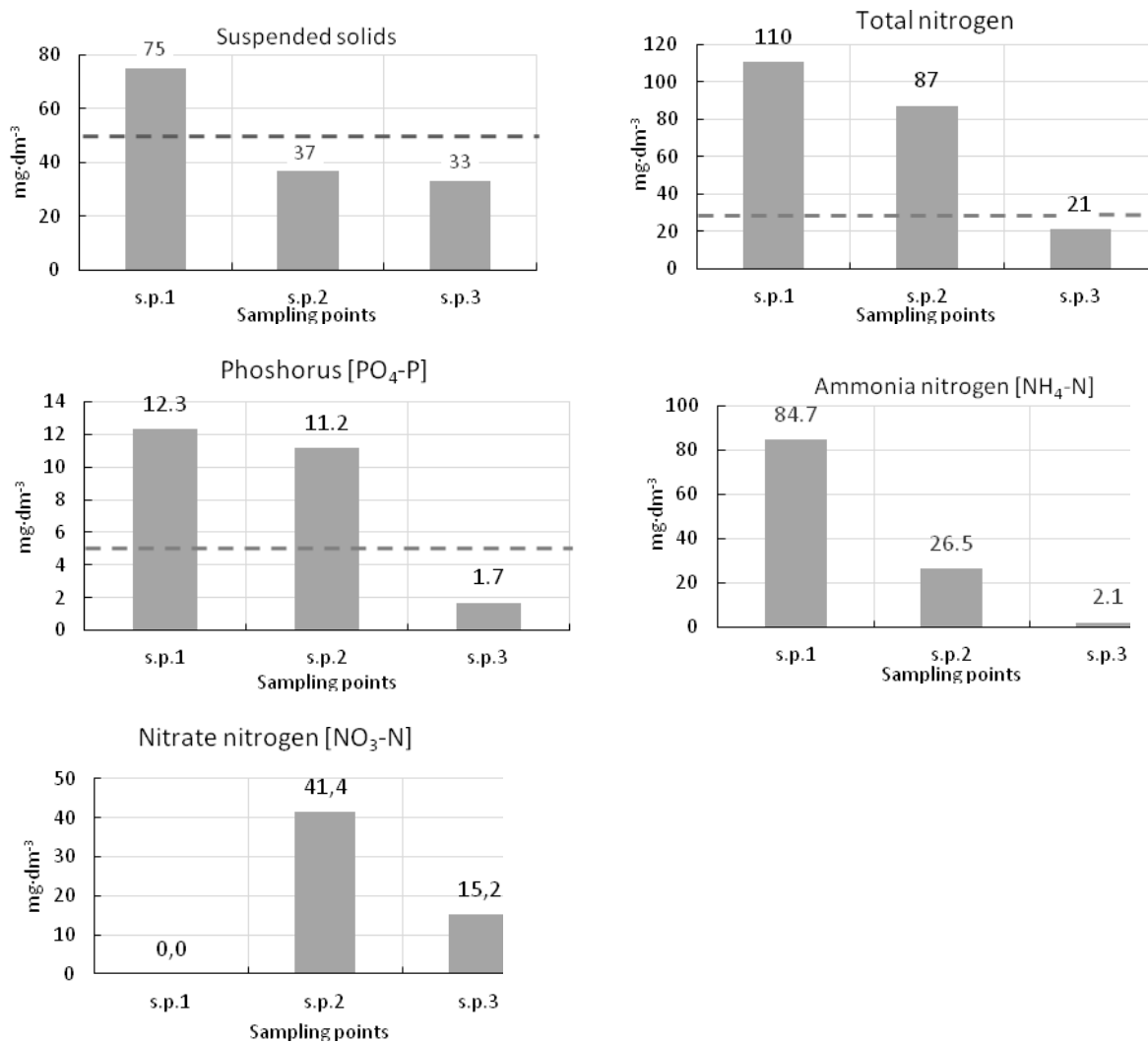


Figure 4. Dynamics of reduction of the mean pollutant concentrations in the successive treatment steps .

Table 5. The specific loads of pollutants in treated wastewater – median values [g·PE⁻¹·d⁻¹]

Specification	Sampling points		
	s.p.1	s.p.2	s.p.3
BOD ₅	35	7	0.4*
COD	354	13	3.8
N _{tot}	16.0	13.4	3.0*
NH ₄ -N	12.6	3.8	0.06
PO ₄ -P	1.7	1.5	0.23*

*HELCOM Recommendation 28E/6 (2007): BOD₅, 8 g·PE⁻¹·d⁻¹; N_{tot}, 10 g·PE⁻¹·d⁻¹; P_{tot}, 0.65 g·PE⁻¹·d⁻¹

Compared to the technological reliabilities of domestic wastewater treatment plants evaluated by other authors (Bugajski et al. 2012, Wałęga et al. 2008), the installation

investigated in this study was much more efficient and reliable as far as the removal of pollutants was concerned. The reliability of reducing the levels of organic matter in wastewater was 100% for BOD₅ and COD and more than 92% for suspended solids. The corresponding values for the treatment plant Biocompact BCT S-12 (with activated sludge) were 68% (BOD), 88% (COD) and 62% (suspended solids) (Bugajski et al. 2012). In the case of the domestic treatment plant RetroFAST (with an aerated biological filter) the reliability values were 85%, 89% and 92%, respectively (Wałęga et al. 2008). Wastewater from individual rural households collected in septic tanks is characterized by several times higher concentrations of pollutants than wastewater discharged by municipal sewage systems. The results of a two-year monitoring study of the quality of wastewater, conducted in one of Polish villages are shown in Table 6.

Table 6. Data on pollutant concentrations in wastewater outflowing from septic tanks in a village in Poland. A two-year monitoring study.

Parameter	Number of samples	Mean	Median	Minimum	Maximum	Standard deviation	Coefficient of variation	Mean values in municipal wastewater
		mg dm ⁻³	mg dm ⁻³	mg dm ⁻³	mg dm ⁻³	mg dm ⁻³	%	mg dm ⁻³
BOD ₅	147	521.1	460.0	100.0	1300.0	236.0	45.3	197
COD	149	866.3	811.0	251.0	1754.0	295.6	34.1	393
Suspended solids	149	205.5	140.0	45.6	3060.0	272.9	132.8	116
Total nitrogen N _{tot}	149	150.1	145.7	28.3	323.5	50.1	33.4	36
Ammonia nitrogen NH ₄ -N	149	109.9	101.9	18.4	280.1	40.3	36.7	25
Phosphorus PO ₄ -P	149	16.5	15.9	2.5	30.7	5.3	32.1	6

Due to this fact, the technological set up of a single-family WWTP (below 50 PE) needs to be characterized by a very high pollutant removal efficiency as well as a very high resistance to the these fluctuations. Such requirements are practically impossible to meet using container WWTPs with activated sludge or trickling filters. By contrast, hybrid systems equipped with beds built as treatment wetlands can easily adapt to such fluctuations and ensure stable removal of pollutants from wastewater.

As far as BOD₅ and COD are concerned, the analyzed installation worked without technological failures over the whole 10-year study period. For suspended solids, the probability of occurrence of failure events (effluent quality parameters higher than permitted)

1 was 2 days per year and for phosphorus 7 days per year. The technological reliability of total
2 nitrogen removal was much lower (76.8%), with as many as 85 failure days during the whole
3 year. The hybrid treatment plant had operated continuously for more than 10-years and had
4 been maintained to ensure constant operational availability. The yearly removal efficiency of
5 pollutants was sensitive only to a slight periodic variability of both hydraulic and pollution
6 loads caused by tourists staying at the farm during vacation periods. The plant had never been
7 observed to freeze in winter thanks to the snow cover, and the only decrease in average
8 efficiency in the cold season concerned the removal of $N_{tot.}$ (18%) (Jucherski & Walczowski
9 2012). These malfunctions occurred in winter when the weather conditions were not
10 conducive to efficient denitrification of NO_3-N , which was the dominant form of nitrogen in
11 the effluent (Fig. 4). By contrast, the installation showed a very high rate of conversion of
12 ammonium nitrogen. The average concentration of NH_4-N did not exceed $2.1 \text{ mg} \cdot \text{dm}^{-3}$ over
13 the entire research period. In order to increase the efficiency of tertiary wastewater treatment
14 in winter seasons and thereby improve the overall pollutant removal efficiency of the WWTP,
15 further efforts have to be made at re-designing and re-building the existing filter bed.
16

17
18 To summarize, the installation tested can be particularly recommended for use in
19 mountainous regions, where streams and rivers as well as underground waters are very
20 sensitive to pollution and, therefore, require higher levels of protection. The high reliability of
21 this type of wastewater treatment plants is a consequence of the application of a hybrid
22 configuration of facilities which is characterized by an increased technological inertia in the
23 multi-staged wastewater treatment process (Jucherski 2007). The number and configuration of
24 the facilities constituting the wastewater treatment installation have been chosen so as to
25 ensure the stability of the process under changeable weather conditions and variable pollutant
26 loads in raw wastewater. The advantages of the investigated installation include simple
27 operation, low power consumption and low operating costs. One disadvantage is that,
28 compared to a container WWTP, the system occupies a slightly larger surface area, which,
29 however, does not limit its application, especially in rural (Nastawny & Jucherski 2013) or
30 protected areas (Jóźwiakowski et al. 2014, Jóźwiakowski et al. 2016). The design
31 and structure of the test facility make it especially suitable for use in sloping terrain with large
32 inclines typical of mountainous regions.
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51

CONCLUSIONS

This study showed that the technological solutions applied in the investigated installation for the treatment of wastewater produced by an eco-tourist mountain farm, proved to be very

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51

effective and reliable during the whole 10-year period of operation. The long-term median concentration values of effluent pollutants ($BOD_5 - 2.5 \text{ mg O}_2 \cdot \text{dm}^{-3}$, $COD - 25.0 \text{ mg O}_2 \cdot \text{dm}^{-3}$, $N_{\text{tot}} - 19.5 \text{ mg} \cdot \text{dm}^{-3}$, $PO_4\text{-P} - 1.5 \text{ mg} \cdot \text{dm}^{-3}$ and suspended solids $- 14.0 \text{ mg} \cdot \text{dm}^{-3}$) were lower than permitted by the Polish Regulation (2014). At the same time, the specific loads of pollutants in the effluent were much lower than those specified in the HELCOM Recommendation.

The technological reliability of the tested installation (100% for both BOD_5 and COD removal, over 90% for the removal of $PO_4\text{-P}$ and total suspended solids, and 77% for total-nitrogen removal) calculated with the Weibull method, confirmed that the treatment plant could be used as an effective tool for protecting the quality of local water resources (especially in ecologically valuable mountainous areas) regardless of changeable weather conditions and variable loads of pollutants characteristic of individual wastewater management in rural regions.

The statistical methods based on the Weibull as well as the lognormal data distributions describe very well the degree of stability and technological reliability of treatment processes, and the differences between them in estimating reliability are negligible.

The Weibull method is especially well-suited for comparing the specific functional features of various types of rural domestic wastewater treatment plants, but the log-normal distribution can also be used.

REFERENCES

- Bugajski, P., Wałęga, A. & Kaczor G. 2012 Application of the Weibull reliability analysis of household sewage treatment plant. *Gaz, Woda i Technika Sanitarna* **2**, 56–58 (in Polish).
- Djeddou, M. & Achour B. 2015. Wastewater treatment plant reliability prediction using artificial neural networks. In: *12th IWA Specialised Conference on Design, Operation and Economics of Large Wastewater Treatment Plants*, September 6-9, 2015, Prague, Czech Republic.
- Eisenberg, D., Soller, J., Sakaji, R. & Olivieri A. 2001 A methodology to evaluate water and wastewater treatment plant reliability. *Water Sci. Technol.* **43** (10), 91–99.
- Gajewska, M., Józwiakowski, K., Ghrabi, A. & Masi F. 2015 Impact of influent wastewater quality on nitrogen removal rates in multistage treatment wetlands. *Environ. Sci. Pollut. Res.* **22**, 12840-1284.

- 1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
- Gizińska-Górna, M., Czekala, W., Józwiakowski, K., Lewicki, A., Dach, J., Marzec, M., Pytka, A., Janczak, D., Kowalczyk-Juško, A., Listosz, A. 2016. The possibility of using plants from hybrid constructed wetland wastewater treatment plants for energy purposes. *Ecol. Eng.* **95**, 534-541.
- HELCOM Recommendation 28E/6. Adopted 15 November 2007 having regard to article 20, Paragraph 1 b) of the Helsinki Convention. *On-site wastewater treatment of single family homes, small businesses and settlements up to 300 Person Equivalent (P.E.)*.
- Jucherski, A. 2007 The quality of farm house-hold wastewater treatment in quasi-technical farmstead installation of IBMER model, in winter period on the mountainous terrain. *Probl. Inż. Rol.* **2 (56)**, 51–60 (in Polish).
- Jucherski, A. & Walczowski A. 2012 Quasi-technical sewage treatment plants in protection of the water resources on rural mountain terrains. *Probl. Inż. Rol.* **3 (77)**, 151–158 (in Polish).
- Józwiakowski, K., Marzec, M., Gizińska-Górna, M., Pytka, A., Skwarzyńska, A., Gajewska, M., Słowik, T., Kowalczyk-Juško, A., Steszuk, A., Grabowski, T. & Szawara, Z. 2014 The concept of construction of hybrid constructed wetland for wastewater treatment in Roztoczański National Park. *Barometr Regionalny* **12 (4)**, 91-102.
- Józwiakowski, K., Mucha, Z., Generowicz, A., Baran, S., Bielińska, J. & Wójcik, W. 2015 The use of multi-criteria analysis for selection of technology for a household WWTP compatible with sustainable development, *Arch. Environ. Prot.* **3**, 76-82.
- Józwiakowski, K., Gajewska, M., Marzec, M., Gizińska-Górna, M., Pytka, A., Kowalczyk-Juško, A., Sosnowska, B., Baran, S., Malik, A., Kufel, R. 2016. *Hybrid constructed wetlands for the National Parks - a case study, requirements, dimensioning, preliminary results*. In: Natural and Constructed Wetlands. Nutrients, heavy metals and energy cycling, and flow. Springer International Publishing Switzerland, Vymazal, J. (Eds.), 247-265.
- Masi, F., Martinuzzi, N., Bresciani, R., Giovannelli, L. & Conte, G. 2007. Tolerance to hydraulic and organic load fluctuations in constructed wetlands. *Water Sci. Technol.* **56 (3)**, 39-48.
- Masi, F., Caffaz, S. & Ghrabi, A. 2013 Multi-stage constructed wetlands systems for municipal wastewater treatment, *Water Sci. Technol.* **67**, 1590–1598.
- Massoud, M. A., Tarhini, A. & Nasr, J. A. 2009 Decentralized approaches to wastewater treatment and management: Applicability in developing countries. *J. Environ. Manage.* **90 (1)**, 652–659.

- 1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
- Nastawny, M. & Jucherski, A. 2013 Assessing technical reliability of an on-site sewage treatment plant with filtration bed system, by using modified Weibull's method. *Probl. Inż. Rol.* **2 (80)**, 165–175 (in Polish).
- Niku, S., Schroeder, E.D. & Haugh, R.S. 1982 Reliability and stability of trickling filter processes. *J. Water Pollut. Control. Fed.* **54 (2)**, 129–134.
- Oliveira, S. C. & Sterling, M. V. 2008 Reliability analysis of wastewater treatment plants. *Water Res.* **42**, 1182–1194.
- Osaliya, R., Kansime, F. Oryem-Origa, H. & Kateyo, E. 2011 The potential use of storm water and effluent from a constructed wetland for re-vegetating a degraded pyrite trail in Queen Elizabeth National Park, Uganda. *Physics and Chemistry of the Earth, Parts A/B/C* **36 (14-15)**, 842-852.
- Platzer, C. & Mauch, K. 1997 Soil clogging in vertical flow reed beds - mechanisms, parameters, consequences and.....solutions? *Water Sci. Technol.* **35 (5)**, 175–181.
- Regulation of the Minister of Environment on 24.07.2014. On the conditions to be met when sewage into water or soil and on substances particularly harmful to the aquatic environment, Dz. U. nr 239 poz. 1800 (in Polish).
- Sanchez-Ramos, D., Sánchez-Emeterio, G. & Beltrán, M. F. 2015 Changes in water quality of treated sewage effluents by their receiving environments in Tablas de Daimiel National Park, Spain. *Environ. Sci. Pollut. Res.* **23 (7)**, 6082-6090.
- Wałęga, A. 2009 Assessment of the wastewater treatment plants statistical methods. *Forum eksploatacja* **5 (44)**, 30–34 (in Polish).
- Wałęga, A., Miernik, W. & Kozień, T. 2008 The efficiency of a domestic sewage treatment plant type RetroFAST. *Przemysł Chemiczny* **87 (5)**, 210–212 (in Polish).
- Wojciechowska, E., Gajewska, M. & Ostojski, A. 2016. Reliability of nitrogen removal processes in multistage treatment wetlands receiving high-strength wastewater, *Ecol. Eng.* **98**, 365-371.

Assessment of the technological reliability of a hybrid constructed wetland for wastewater treatment in a mountain eco-tourist farm in Poland

Andrzej Jucherski¹, Maria Nastawny¹, Andrzej Walczowski¹,
Krzysztof Józwiakowski² and Magdalena Gajewska³

¹*Mountain Centre of Studies and Implementations in Tylicz, Institute of Technology and Life Sciences
in Falenty, Pułaskiego St. 25A, 33-383 Tylicz, POLAND*

²*Department of Environmental Engineering and Geodesy, University of Life Sciences in Lublin,
Leszczyńskiego 7, 20-069 Lublin, POLAND (krzysztof.jozwiakowski@up.lublin.pl)*

³*Department of Water and Wastewater Technology, Gdańsk University of Technology, Narutowicza st.
11/12, 80-233, Gdańsk, POLAND*

ABSTRACT

The aim of the present study was to assess the technological reliability of a domestic hybrid wastewater treatment installation consisting of a classic three-chambered (volume 6m³) septic tank, a vertical flow (VF) trickling bed filled with granules of a calcinated clay material (KERAMZYT), a special wetland bed constructed on a slope, and a permeable pond used as a receiver. The test treatment plant was located at a mountain eco-tourist farm on the periphery of the spa municipality of Krynica-Zdrój, Poland. The plant's operational reliability in reducing the concentration of organic matter measured as BOD₅ and COD, was 100% when modelled by both the Weibull and the lognormal distributions. The respective reliability values for total nitrogen removal were 76.8% and 77.0%, total suspended solids – 99.5% and 92.6 %, and PO₄-P – 98.2% and 95.2%, with the differences being negligible. The installation was characterized by a very high level of technological reliability when compared to other solutions of this type. The Weibull method employed for statistical evaluation of technological reliability can also be used for comparison purposes. From the ecological perspective, the facility presented in the study has proven to be an effective tool for protecting local aquifer areas.

Key words: mountain aquifers, rural areas, cold climate, hybrid constructed wetland, technological reliability

INTRODUCTION

Evaluation of the technological reliability of individual wastewater treatment systems should be an important part of planning and decision-making in water and wastewater management, particularly now, when a wide range of technological solutions are available (Józwiakowski et al. 2015). Reliable operation of wastewater treatment units must be ensured due to both environmental and human health protection concerns (Eisenberg et al. 2001; Wojciechowska et al 2016). Reliable operation of domestic wastewater treatment plants is especially important in mountain aquifer areas, which are very sensitive to pollution. Mountainous regions in Poland play a key role in developing and sustaining vital socio-economical and environmental functions which intertwine in the activities of spa and tourist resorts, forest management, environment-friendly farming and especially in hydrology.

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
Although Polish mountainous areas have a high water production potential, as manifested by an almost 40% regional surplus in relation to the water discharged by all the rivers, Poland occupies one of the last positions in Europe in terms of the total freshwater resources, which are estimated at 1630 m³·year⁻¹·person⁻¹. Therefore, it is essential that groundwater and the upper reaches of local streams and mountain rivers should be protected against biological, chemical and bacteriological pollution resulting from the discharge of untreated domestic sewage to the environment in rural areas. One of the key issues in technological progress in wastewater management in rural, environmentally valuable areas, is the construction of small domestic or local wastewater treatment plants with a high, long-term reliability and effectiveness in reducing wastewater pollutions (Jucherski & Walczowski 2012; Masi et al. 2013; Józwiakowski et al. 2016; Gajewska et al. 2015).

Nowadays, more and more innovative wastewater treatment systems are being designed and offered on the market, which spurs the need for developing a universal method of assessing the reliability of the various treatment processes and facilities. Such a method would be helpful in planning and comparing the levels of protection offered by the various technologies (Józwiakowski et al. 2015).

The methods for determining the reliability of individual wastewater treatment systems have been described in more detail by Eisenberg et al. (2001). Lately Djeddou & Achour (2015) have proposed a method for predicting reliability using artificial neural networks.

A comprehensive and useful assessment of the reliability of domestic wastewater treatment plants should be based on a series of measurements and observations of treatment variability under normal and critical operating conditions as well as the probability of mechanical failures and their impact on the quality of the treated wastewater (Eisenberg et al. 2001).

Reliability is defined as the probability of achieving required performance of a wastewater treatment plant (WWTP) over a specific time and under specific conditions (Oliveira & Sterling 2008). To assess WWTP, a coefficient of reliability (CR) which relates mean pollutant concentrations to effluent standards (Niku et al. 1982) can also be used.

The statistical step in the assessment of WWTP reliability presented in this article is based on the normal (Niku et al. 1982), the lognormal (Oliveira & Sterling 2008) and the Weibull distributions (Bugajski et al. 2012; Nastawny & Jucherski 2013; Wałęga 2009). Statistical distributions of probability are used to establish the probability of occurrence of selected values of pollutants. Recent findings reported in the literature (Bugajski et al. 2012; Bugajski

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60
61
62
63
64
65
66
67
68
69
70
71
72
73
74
75
76
77
78
79
80
81
82
83
84
85
86
87
88
89
90
91
92
93
94
95
96
97
98
99
100
101
102
103
104
105
106
107
108
109
110
111
112
113
114
115
116
117
118
119
120
121
122
123
124
125
126
127
128
129
130
131
132
133
134
135
136
137
138
139
140
141
142
143
144
145
146
147
148
149
150
151
152
153
154
155
156
157
158
159
160
161
162
163
164
165
166
167
168
169
170
171
172
173
174
175
176
177
178
179
180
181
182
183
184
185
186
187
188
189
190
191
192
193
194
195
196
197
198
199
200
201
202
203
204
205
206
207
208
209
210
211
212
213
214
215
216
217
218
219
220
221
222
223
224
225
226
227
228
229
230
231
232
233
234
235
236
237
238
239
240
241
242
243
244
245
246
247
248
249
250
251
252
253
254
255
256
257
258
259
260
261
262
263
264
265
266
267
268
269
270
271
272
273
274
275
276
277
278
279
280
281
282
283
284
285
286
287
288
289
290
291
292
293
294
295
296
297
298
299
300
301
302
303
304
305
306
307
308
309
310
311
312
313
314
315
316
317
318
319
320
321
322
323
324
325
326
327
328
329
330
331
332
333
334
335
336
337
338
339
340
341
342
343
344
345
346
347
348
349
350
351
352
353
354
355
356
357
358
359
360
361
362
363
364
365
366
367
368
369
370
371
372
373
374
375
376
377
378
379
380
381
382
383
384
385
386
387
388
389
390
391
392
393
394
395
396
397
398
399
400
401
402
403
404
405
406
407
408
409
410
411
412
413
414
415
416
417
418
419
420
421
422
423
424
425
426
427
428
429
430
431
432
433
434
435
436
437
438
439
440
441
442
443
444
445
446
447
448
449
450
451
452
453
454
455
456
457
458
459
460
461
462
463
464
465
466
467
468
469
470
471
472
473
474
475
476
477
478
479
480
481
482
483
484
485
486
487
488
489
490
491
492
493
494
495
496
497
498
499
500
501
502
503
504
505
506
507
508
509
510
511
512
513
514
515
516
517
518
519
520
521
522
523
524
525
526
527
528
529
530
531
532
533
534
535
536
537
538
539
540
541
542
543
544
545
546
547
548
549
550
551
552
553
554
555
556
557
558
559
560
561
562
563
564
565
566
567
568
569
570
571
572
573
574
575
576
577
578
579
580
581
582
583
584
585
586
587
588
589
590
591
592
593
594
595
596
597
598
599
600
601
602
603
604
605
606
607
608
609
610
611
612
613
614
615
616
617
618
619
620
621
622
623
624
625
626
627
628
629
630
631
632
633
634
635
636
637
638
639
640
641
642
643
644
645
646
647
648
649
650
651
652
653
654
655
656
657
658
659
660
661
662
663
664
665
666
667
668
669
670
671
672
673
674
675
676
677
678
679
680
681
682
683
684
685
686
687
688
689
690
691
692
693
694
695
696
697
698
699
700
701
702
703
704
705
706
707
708
709
710
711
712
713
714
715
716
717
718
719
720
721
722
723
724
725
726
727
728
729
730
731
732
733
734
735
736
737
738
739
740
741
742
743
744
745
746
747
748
749
750
751
752
753
754
755
756
757
758
759
760
761
762
763
764
765
766
767
768
769
770
771
772
773
774
775
776
777
778
779
780
781
782
783
784
785
786
787
788
789
790
791
792
793
794
795
796
797
798
799
800
801
802
803
804
805
806
807
808
809
810
811
812
813
814
815
816
817
818
819
820
821
822
823
824
825
826
827
828
829
830
831
832
833
834
835
836
837
838
839
840
841
842
843
844
845
846
847
848
849
850
851
852
853
854
855
856
857
858
859
860
861
862
863
864
865
866
867
868
869
870
871
872
873
874
875
876
877
878
879
880
881
882
883
884
885
886
887
888
889
890
891
892
893
894
895
896
897
898
899
900
901
902
903
904
905
906
907
908
909
910
911
912
913
914
915
916
917
918
919
920
921
922
923
924
925
926
927
928
929
930
931
932
933
934
935
936
937
938
939
940
941
942
943
944
945
946
947
948
949
950
951
952
953
954
955
956
957
958
959
960
961
962
963
964
965
966
967
968
969
970
971
972
973
974
975
976
977
978
979
980
981
982
983
984
985
986
987
988
989
990
991
992
993
994
995
996
997
998
999
1000

2014; Nastawny & Jucherski 2013; Wałęga 2009) show that the Weibull distribution is an accurate and precise tool for evaluation of WWTP reliability.

Systems for domestic wastewater management are individual facilities with technical and quasi-technical treatment devices designed to collect and treat wastewater to the extent required by specific regulations (Regulation of the Polish Minister of Environment 2014) as well as discharge it to receivers without adversely affecting the soil–water complex in the place where the facilities are located. In rural areas, individual treatment facilities usually operate without constant supervision and are therefore particularly exposed to fluctuations in efficiency due to a variable load pattern (Massoud et al. 2009; Platzer & Mauch 1997); in consequence, the quality of effluent often does not meet the requirements stipulated in the regulations in force.

Hybrid wetland systems have recently been more and more frequently used for the treatment of domestic wastewater from museum buildings and forester or mountain shelters, including those located in national parks. When well designed and properly maintained, they can achieve high pollutant removal efficiencies (Masi et al. 2007; Osaliya et al. 2011; Józwiakowski et al. 2014; Sanchez-Ramos et al. 2015; Gizińska-Górna et. 2016; Józwiakowski et al. 2016). The literature, however, provides little data on the reliability of pollutant removal processes in such CWS over long periods (years) of operation.

The aim of the present study was to assess the range of long-term fluctuations in treatment reliability in a domestic hybrid wastewater treatment plant. The plant had been built over ten years before on an eco-tourist farm in the mountain municipality and spa of Krynica-Zdrój in Poland and had been continuously operating since that time. The following indicators of wastewater contamination were measured: (i) BOD₅ and COD for contamination with organic matter, (ii) total suspended solids, (iii) total nitrogen (TN), and (iv) phosphorus PO₄-P. The indicators results (pollutant concentrations) were compared to the Polish standards for treated wastewater (Regulation of the Polish Minister of Environment 2014) discharged into water and soil from treatment plants below 2000 PE.

MATERIAL AND METHODS

The subject of the study was a hybrid wastewater treatment plant described in detail by Jucherski & Walczowski (2012). The plant was operated by an eco-tourist farm located in the rural peripheries of the spa town of Krynica-Zdrój, Poland. The plant had been monitored over the years 2005–2015. A schematic of the facility with the sampling points is presented in Fig. 1.

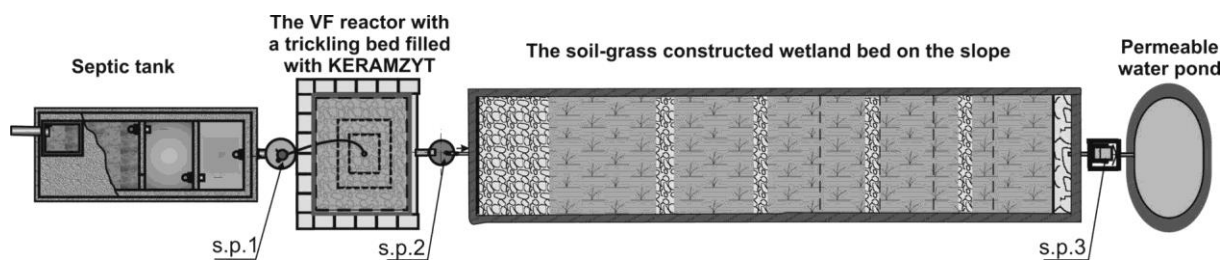


Figure 1. Schematic of the wastewater treatment installation (sampling points: s.p.1, s.p.2, s.p.3)

The installation consisted of a classic three-chamber septic tank, a vertical flow reactor (filter) followed by a special constructed wetland (SCW), and a permeable water pond as a receiver of the final effluent. The septic tank, with a capacity of 6m^3 , was a monolithic concrete structure designed to receive sewage with a seasonal variability from 3 to 15 persons (with an average of $\text{PE}=5$). The substrate used in the vertical flow reactor were granules of a sintered clay material (KERAMZYT). To improve biological treatment and nitrification at the vertical stage, the wastewater was sprayed onto the surface of the reactor. Due to the harsh climate, it was necessary to use a cover to insulate the reactor from freezing in winter. Downstream of the reactor, there was a special filter bed (wetland) with subsurface flow, planted with a mix of reed sweet grass (*Glyceria maxima*), reed canary grass (*Phalaris arundinacea*) and other grasses spontaneously inhabiting the bed. The bed was constructed on a slope for tertiary treatment and removal of the remaining nutrients (N and P). The installation ended with a permeable pond for receiving and infiltration of the treated wastewater into the soil complex surrounding the treatment unit.

The average hydraulic load of the treatment plant in the investigation period was $621.2\text{ dm}^3\cdot\text{day}^{-1}$, and the average concentrations of pollutants in raw sewage were $271.7\text{ mg O}_2\cdot\text{dm}^{-3}$ for BOD_5 , $390.8\text{ mg O}_2\cdot\text{dm}^{-3}$ for COD, $75.4\text{ mg}\cdot\text{dm}^{-3}$ for total suspended solids, $110.5\text{ mg}\cdot\text{dm}^{-3}$ for total nitrogen, and $12.3\text{ mg}\cdot\text{dm}^{-3}$ for phosphorus $\text{PO}_4\text{-P}$ (Table 1). The flow of treated wastewater was calculated based on the water consumption reading of a water meter. BOD_5 was determined using the OxiTop respirometric measuring system from WTW. COD, total nitrogen and phosphate phosphorus were determined using a Merck SQ118 photometer and a Merck thermoreactor TR-200. The total suspended solids were determined by a gravimetric method, in accordance with the standard PN-72/C-04559/02.

The statistical analysis was based on the normal, lognormal and Weibull distributions. Statistica v. 13.0 software was employed to define the characteristics of the distribution of the empirical data using the Kolmogorov-Smirnov goodness-of-fit test. Data were tested for

normality of distribution by measuring the distance between the empirical distribution and the theoretical distribution. The following null hypothesis was tested at 0.05 level of significance: distribution of the variable is normal/lognormal/Weibull. Furthermore the quality of fit of the Weibull distribution to empirical data was assessed using the Hollander–Proschan test for the significance level of 0.05. The reliability function $R(x)$ was calculated as a complement to the cumulative distribution function using the following formula:

$$R(x) = 1 - F(x) \quad [1]$$

where x is an indicator of the concentration of pollutants in treated wastewater (Bugajski et al. 2012).

Reliability was determined from cumulative distribution plots, taking into consideration pollutant concentrations in treated wastewater permitted by the Regulation of the Polish Minister of Environment (2014), i.e.: $BOD_5 \leq 40 \text{ mg O}_2 \cdot \text{dm}^{-3}$, $COD \leq 150 \text{ mg O}_2 \cdot \text{dm}^{-3}$, total suspended solids $\leq 50 \text{ mg} \cdot \text{dm}^{-3}$, total nitrogen $\leq 30 \text{ mg} \cdot \text{dm}^{-3}$, total phosphorus $\leq 5 \text{ mg} \cdot \text{dm}^{-3}$.

RESULTS AND DISCUSSION

The many-year means of effluent contaminant concentrations in wastewater treated in the investigated installation ($BOD_5 - 3.49 \text{ mgO}_2 \cdot \text{dm}^{-3}$, $COD - 28.0 \text{ mgO}_2 \cdot \text{dm}^{-3}$, suspended solids $- 15.8 \text{ mg} \cdot \text{dm}^{-3}$, total nitrogen $- 20.9 \text{ mg} \cdot \text{dm}^{-3}$, and phosphorus $P-PO_4 - 1.70 \text{ mg} \cdot \text{dm}^{-3}$) (Table 1) were much lower than required by the Regulation (2014) on discharging wastewater into the soil or surface waters including lakes and their tributaries, and artificial water reservoirs situated on flowing waters.

Table 1 shows the basic statistics for pollutant concentration in wastewater.

Table 1. Basic statistics for pollutant concentrations in wastewater

Parameter		Number of samples	Mean	Median	Minimum	Maximum	Standard deviation	Coefficient of variation
			$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	$\text{mg} \cdot \text{dm}^{-3}$	%
BOD_5	inlet	57	271.7	230	90	580	132.9	48.8
	outlet	49	3.49	2.5	0	13	2.92	83.6
COD	inlet	61	391	353	214	641	114.9	29.4
	outlet	55	28	25	5	112	17.6	63
Suspended solids	inlet	48	75.4	66	19	218.6	40.5	53.7
	outlet	41	15.8	14	0	44.6	10.9	69.2
Total nitrogen N_{tot}	inlet	61	110.5	105.5	70.3	193.8	19.5	17.6
	outlet	55	20.9	19.5	1.6	64.8	16.4	78.5
Phosphorus $PO_4\text{-P}$	inlet	65	12.3	11.1	7.6	24.9	3.97	32.3
	outlet	59	1.7	1.5	0.14	5.46	1.23	72.2

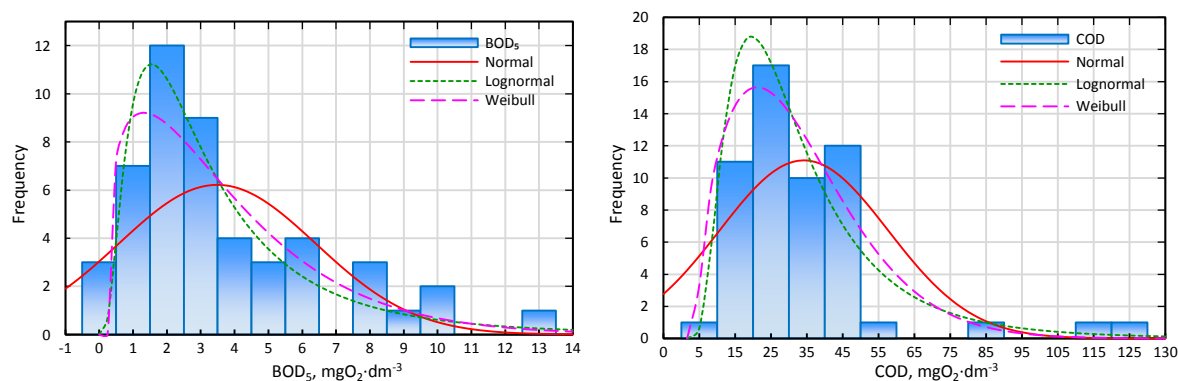
The effluent quality indicators were characterized by high coefficients of variation (Table 1) which, though statistically significant (and therefore useful for the evaluation of the treatment processes in the installation), were too low to have any relevance from the point of view of environmental protection. To determine the technological reliability of the treatment plant, a detailed statistical analysis was performed based on the distributions of the empirical data of each effluent contaminant. The normal, lognormal and Weibull distributions (Table 2, Fig. 2) were adjusted to data sets obtained during the 10-year study.

Table 2. The Kolmogorov-Smirnov goodness-of-fit statistics and significance levels for the analyzed empirical distributions

Distribution	Normal		Lognormal		Weibull	
	stat	p	stat	p	stat	p
BOD ₅	0.2076	0.0324	0.1118	0.5751	0.1354	0.3371
COD	0.1388	0.2183	0.0970	0.6427	0.1157	0.4208
TSS	0.0944	0.8454	0.1416	0.3786	0.1067	0.7262
Total nitrogen N _{tot}	0.1422	0.1960	0.1604	0.1056	0.1085	0.5028
Phosphorus PO ₄ -P	0.1093	0.4501	0.0926	0.6585	0.0507	0.9962

Symbols: stat – value of the statistic test, p – significance level of the test; when p is greater than 0.05, the distribution of empirical data can be described by the analyzed distribution

Statistical analysis using the Kolmogorov-Smirnov goodness-of-fit test showed that the Weibull and lognormal distributions could be well fitted to the empirical distributions of each pollution indicator, whereas the normal distribution gave a much worse fit, although it could also be used for most of the parameters, except BOD₅ (Table 2).



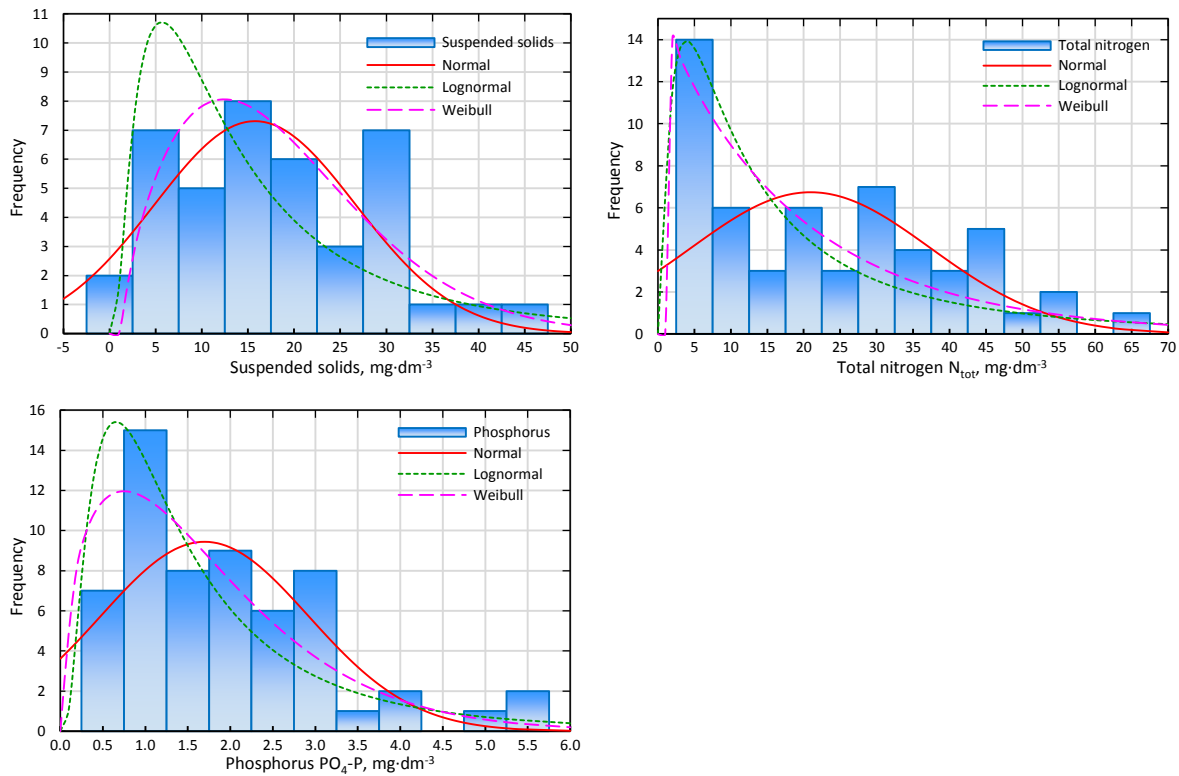


Figure 2. Histograms of the normal, lognormal and Weibull distributions of the empirical data

Based on the detailed analysis and evaluation of the WWTP, as reported above, its reliability was modelled using the Weibull distribution (Table 3, Fig. 3). This allowed us to compare our results with those obtained by other authors (Bugajski et al. 2012; Nastawny & Jucherski 2013; Wałęga 2009) who had used the same distribution. In addition, the indicators of the technological reliability of the treatment plant were also compared to values obtained from the lognormal distribution. The parameters of the Weibull distribution were calculated using the maximum likelihood estimation. In order to determine the goodness of fit of the Weibull distribution to the empirical data described by the distribution parameters (Table 3), the Hollander–Proschan test was applied. As can be seen from Table 3, the goodness of fit of the obtained distributions was high and ranged from 72 to 98% at a significance level of 0.05 (Table 3).

Table 3. Parameters of the Weibull distribution and the Hollander–Proschan goodness-of-fit test

Parameter	Parameters of Weibull distribution			Hollander–Proschan goodness-of-fit test	
	Location	Shape	Scale	stat	p
BOD ₅	0.3182	1.2479	3.6602	0.2150	0.8297
COD	2.4697	1.5798	28.5112	0.0200	0.9840
Suspended solids	-0.6212	1.6638	19.2133	-0.1235	0.9017
Total nitrogen N _{tot}	1.2364	0.9844	19.5929	-0.3558	0.7220
Phosphorus PO ₄ -P	0.0707	1.3664	1.7796	0.0411	0.9672

Symbols: stat - value of the statistic test, p - significance level of the test; when $p \leq 0.05$ the distribution of data is not Weibull distribution

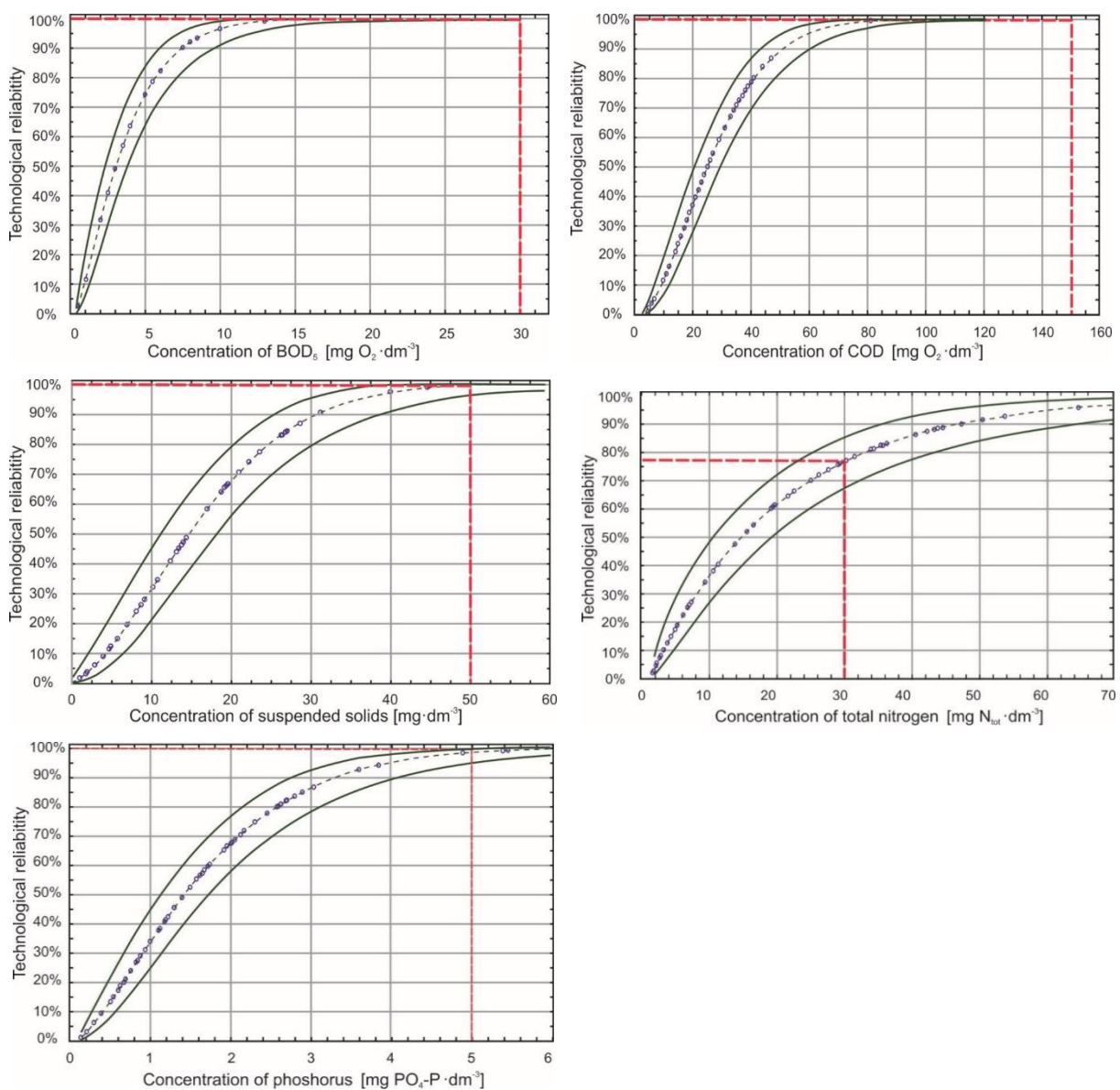


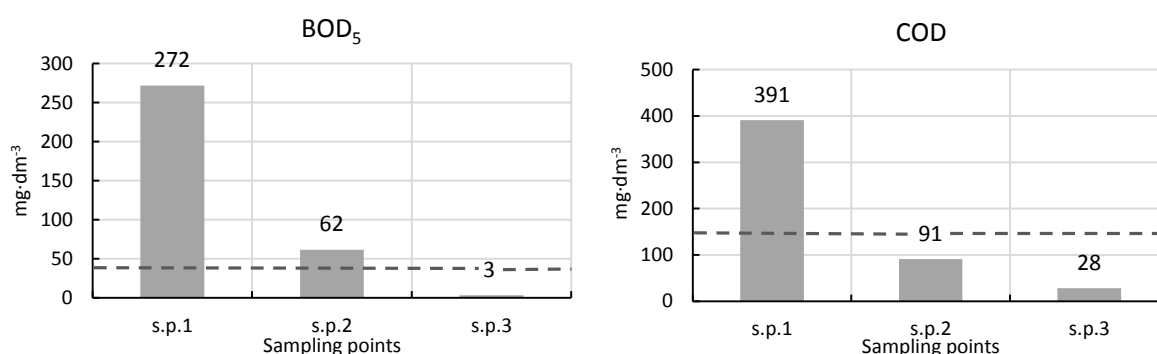
Figure 3. Weibull cumulative distribution functions and the technological reliabilities determined for each pollution parameter with estimated confidence intervals of 95.0%

The technological reliabilities of the installation determined by the Weibull distribution function compared to the lognormal distribution are given in Table 4. It was shown that the reliability of reducing BOD₅ and COD concentrations was 100% both for the lognormal as well as the Weibull distribution functions. For other pollutants, the reliabilities of the treatment plant described by the lognormal distribution and the Weibull distribution were slightly lower at 92.6% and 99.5% for TSS, 77.0% and 76.8% for N_{tot}, and 95.2% and 98.2% for phosphorus PO₄-P, respectively (Fig. 3, Table 4).

Table 4. The technological reliability of the facility for wastewater treatment [in %] determined using the Weibull and the lognormal distribution functions

Parameter	Weibull distribution	Lognormal distribution
BOD ₅	100	100
COD	100	100
Suspended solids	99.5	92.6
Total nitrogen N _{tot}	76.8	77.0
Phosphorus PO ₄ -P	98.2	95.2

The results of this study demonstrate that the wastewater treatment processes were stable and reliable as well as very effective. As shown by the graphs in Figure 4 and the Helsinki Commission Recommendation (HELCOM 2007) data in Table 5, the average values of the parameters of the treated wastewater met the Polish requirements (Regulation of the Polish Minister of Environment 2014). Therefore, treated wastewater could be discharged into the environment throughout the year, with soil receiver sites being preferred over other receiver bodies.



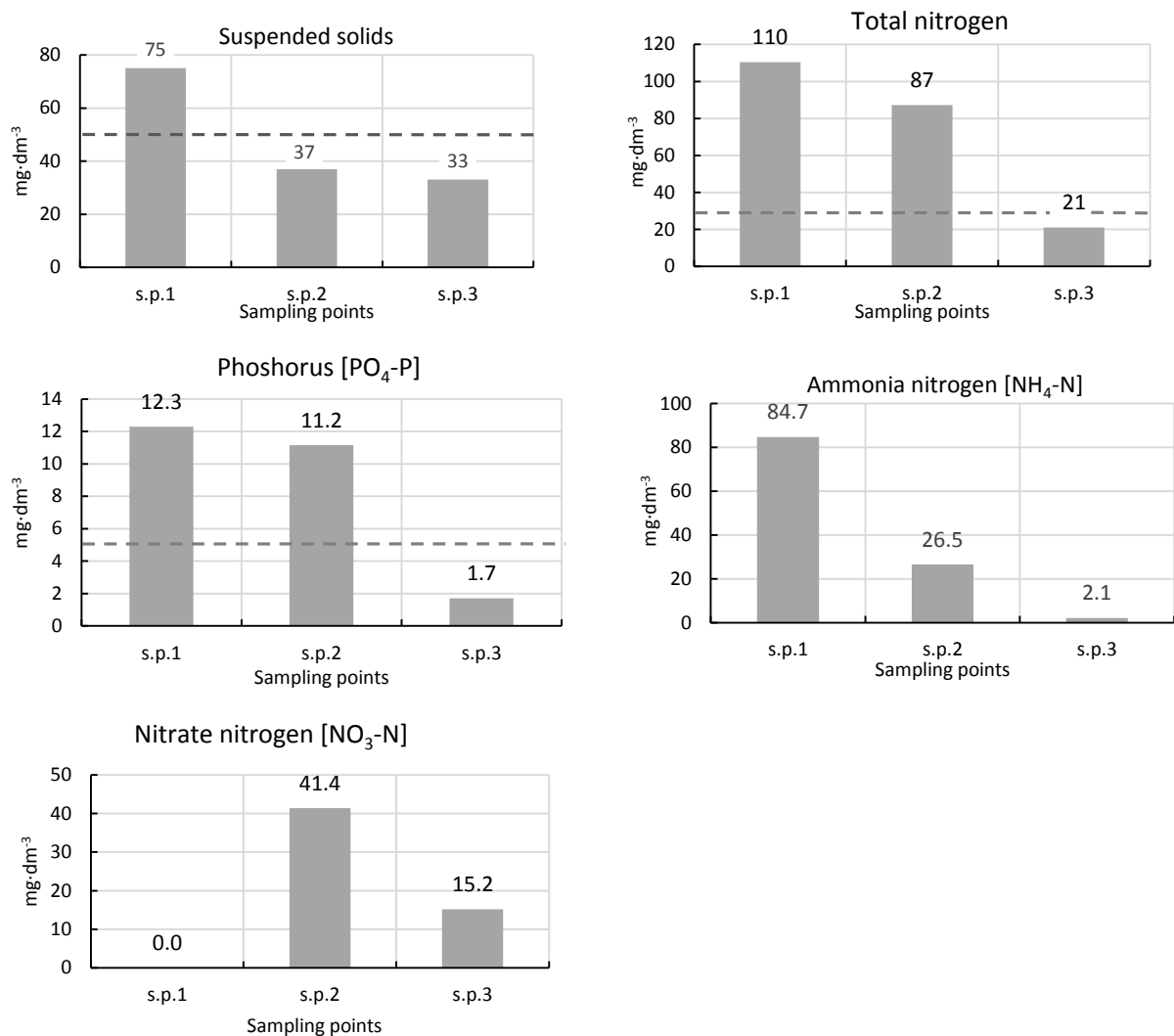


Figure 4. Dynamics of reduction of the mean pollutant concentrations in the successive treatment steps .

Table 5. The specific loads of pollutants in treated wastewater – median values [g·PE⁻¹·d⁻¹]

Specification	Sampling points		
	s.p.1	s.p.2	s.p.3
BOD ₅	35	7	0.4*
COD	354	13	3.8
N _{tot}	16.0	13.4	3.0*
NH ₄ -N	12.6	3.8	0.06
PO ₄ -P	1.7	1.5	0.23*

*HELCOM Recommendation 28E/6 (2007): BOD₅, 8 g·PE⁻¹·d⁻¹; N_{tot}, 10 g·PE⁻¹·d⁻¹; P_{tot}, 0.65 g·PE⁻¹·d⁻¹

Compared to the technological reliabilities of domestic wastewater treatment plants evaluated by other authors (Bugajski et al. 2012, Wałęga et al. 2008), the installation

investigated in this study was much more efficient and reliable as far as the removal of pollutants was concerned. The reliability of reducing the levels of organic matter in wastewater was 100% for BOD₅ and COD and more than 92% for suspended solids. The corresponding values for the treatment plant Biocompact BCT S-12 (with activated sludge) were 68% (BOD), 88% (COD) and 62% (suspended solids) (Bugajski et al. 2012). In the case of the domestic treatment plant RetroFAST (with an aerated biological filter) the reliability values were 85%, 89% and 92%, respectively (Wałęga et al. 2008). Wastewater from individual rural households collected in septic tanks is characterized by several times higher concentrations of pollutants than wastewater discharged by municipal sewage systems. The results of a two-year monitoring study of the quality of wastewater, conducted in one of Polish villages are shown in Table 6.

Table 6. Data on pollutant concentrations in wastewater outflowing from septic tanks in a village in Poland. A two-year monitoring study.

Parameter	Number of samples	Mean	Median	Minimum	Maximum	Standard deviation	Coefficient of variation	Mean values in municipal wastewater
		mg dm ⁻³	mg dm ⁻³	mg dm ⁻³	mg dm ⁻³	mg dm ⁻³	%	mg dm ⁻³
BOD ₅	147	521.1	460.0	100.0	1300.0	236.0	45.3	197
COD	149	866.3	811.0	251.0	1754.0	295.6	34.1	393
Suspended solids	149	205.5	140.0	45.6	3060.0	272.9	132.8	116
Total nitrogen N _{tot}	149	150.1	145.7	28.3	323.5	50.1	33.4	36
Ammonia nitrogen NH ₄ -N	149	109.9	101.9	18.4	280.1	40.3	36.7	25
Phosphorus PO ₄ -P	149	16.5	15.9	2.5	30.7	5.3	32.1	6

Due to this fact, the technological set up of a single-family WWTP (below 50 PE) needs to be characterized by a very high pollutant removal efficiency as well as a very high resistance to these fluctuations. Such requirements are practically impossible to meet using container WWTPs with activated sludge or trickling filters. By contrast, hybrid systems equipped with beds built as treatment wetlands can easily adapt to such fluctuations and ensure stable removal of pollutants from wastewater.

As far as BOD₅ and COD are concerned, the analyzed installation worked without technological failures over the whole 10-year study period. For suspended solids, the probability of occurrence of failure events (effluent quality parameters higher than permitted)

1 was 2 days per year and for phosphorus 7 days per year. The technological reliability of total
2 nitrogen removal was much lower (76.8%), with as many as 85 failure days during the whole
3 year. The hybrid treatment plant had operated continuously for more than 10-years and had
4 been maintained to ensure constant operational availability. The yearly removal efficiency of
5 pollutants was sensitive only to a slight periodic variability of both hydraulic and pollution
6 loads caused by tourists staying at the farm during vacation periods. The plant had never been
7 observed to freeze in winter thanks to the snow cover, and the only decrease in average
8 efficiency in the cold season concerned the removal of $N_{tot.}$ (18%) (Jucherski & Walczowski
9 2012). These malfunctions occurred in winter when the weather conditions were not
10 conducive to efficient denitrification of NO_3-N , which was the dominant form of nitrogen in
11 the effluent (Fig. 4). By contrast, the installation showed a very high rate of conversion of
12 ammonium nitrogen. The average concentration of NH_4-N did not exceed $2.1 \text{ mg} \cdot \text{dm}^{-3}$ over
13 the entire research period. In order to increase the efficiency of tertiary wastewater treatment
14 in winter seasons and thereby improve the overall pollutant removal efficiency of the WWTP,
15 further efforts have to be made at re-designing and re-building the existing filter bed.
16

17
18 To summarize, the installation tested can be particularly recommended for use in
19 mountainous regions, where streams and rivers as well as underground waters are very
20 sensitive to pollution and, therefore, require higher levels of protection. The high reliability of
21 this type of wastewater treatment plants is a consequence of the application of a hybrid
22 configuration of facilities which is characterized by an increased technological inertia in the
23 multi-staged wastewater treatment process (Jucherski 2007). The number and configuration of
24 the facilities constituting the wastewater treatment installation have been chosen so as to
25 ensure the stability of the process under changeable weather conditions and variable pollutant
26 loads in raw wastewater. The advantages of the investigated installation include simple
27 operation, low power consumption and low operating costs. One disadvantage is that,
28 compared to a container WWTP, the system occupies a slightly larger surface area, which,
29 however, does not limit its application, especially in rural (Nastawny & Jucherski 2013) or
30 protected areas (Jóźwiakowski et al. 2014, Jóźwiakowski et al. 2016). The design
31 and structure of the test facility make it especially suitable for use in sloping terrain with large
32 inclines typical of mountainous regions.
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51

CONCLUSIONS

This study showed that the technological solutions applied in the investigated installation for the treatment of wastewater produced by an eco-tourist mountain farm, proved to be very



1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51

effective and reliable during the whole 10-year period of operation. The long-term median concentration values of effluent pollutants ($BOD_5 - 2.5 \text{ mg O}_2 \cdot \text{dm}^{-3}$, $COD - 25.0 \text{ mg O}_2 \cdot \text{dm}^{-3}$, $N_{\text{tot}} - 19.5 \text{ mg} \cdot \text{dm}^{-3}$, $PO_4\text{-P} - 1.5 \text{ mg} \cdot \text{dm}^{-3}$ and suspended solids $- 14.0 \text{ mg} \cdot \text{dm}^{-3}$) were lower than permitted by the Polish Regulation (2014). At the same time, the specific loads of pollutants in the effluent were much lower than those specified in the HELCOM Recommendation.

The technological reliability of the tested installation (100% for both BOD_5 and COD removal, over 90% for the removal of $PO_4\text{-P}$ and total suspended solids, and 77% for total-nitrogen removal) calculated with the Weibull method, confirmed that the treatment plant could be used as an effective tool for protecting the quality of local water resources (especially in ecologically valuable mountainous areas) regardless of changeable weather conditions and variable loads of pollutants characteristic of individual wastewater management in rural regions.

The statistical methods based on the Weibull as well as the lognormal data distributions describe very well the degree of stability and technological reliability of treatment processes, and the differences between them in estimating reliability are negligible.

The Weibull method is especially well-suited for comparing the specific functional features of various types of rural domestic wastewater treatment plants, but the log-normal distribution can also be used.

REFERENCES

- Bugajski, P., Wałęga, A. & Kaczor G. 2012 Application of the Weibull reliability analysis of household sewage treatment plant. *Gaz, Woda i Technika Sanitarna* **2**, 56–58 (in Polish).
- Djeddou, M. & Achour B. 2015. Wastewater treatment plant reliability prediction using artificial neural networks. In: *12th IWA Specialised Conference on Design, Operation and Economics of Large Wastewater Treatment Plants, September 6-9, 2015, Prague, Czech Republic*.
- Eisenberg, D., Soller, J., Sakaji, R. & Olivieri A. 2001 A methodology to evaluate water and wastewater treatment plant reliability. *Water Sci. Technol.* **43** (10), 91–99.
- Gajewska, M., Józwiakowski, K., Ghrabi, A. & Masi F. 2015 Impact of influent wastewater quality on nitrogen removal rates in multistage treatment wetlands. *Environ. Sci. Pollut. Res.* **22**, 12840-1284.

- 1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
- Gizińska-Górna, M., Czekala, W., Józwiakowski, K., Lewicki, A., Dach, J., Marzec, M., Pytka, A., Janczak, D., Kowalczyk-Juško, A., Listosz, A. 2016. The possibility of using plants from hybrid constructed wetland wastewater treatment plants for energy purposes. *Ecol. Eng.* **95**, 534-541.
- HELCOM Recommendation 28E/6. Adopted 15 November 2007 having regard to article 20, Paragraph 1 b) of the Helsinki Convention. *On-site wastewater treatment of single family homes, small businesses and settlements up to 300 Person Equivalent (P.E.)*.
- Jucherski, A. 2007 The quality of farm house-hold wastewater treatment in quasi-technical farmstead installation of IBMER model, in winter period on the mountainous terrain. *Probl. Inż. Rol.* **2 (56)**, 51–60 (in Polish).
- Jucherski, A. & Walczowski A. 2012 Quasi-technical sewage treatment plants in protection of the water resources on rural mountain terrains. *Probl. Inż. Rol.* **3 (77)**, 151–158 (in Polish).
- Józwiakowski, K., Marzec, M., Gizińska-Górna, M., Pytka, A., Skwarzyńska, A., Gajewska, M., Słowik, T., Kowalczyk-Juško, A., Steszuk, A., Grabowski, T. & Szawara, Z. 2014 The concept of construction of hybrid constructed wetland for wastewater treatment in Roztoczański National Park. *Barometr Regionalny* **12 (4)**, 91-102.
- Józwiakowski, K., Mucha, Z., Generowicz, A., Baran, S., Bielińska, J. & Wójcik, W. 2015 The use of multi-criteria analysis for selection of technology for a household WWTP compatible with sustainable development, *Arch. Environ. Prot.* **3**, 76-82.
- Józwiakowski, K., Gajewska, M., Marzec, M., Gizińska-Górna, M., Pytka, A., Kowalczyk-Juško, A., Sosnowska, B., Baran, S., Malik, A., Kufel, R. 2016. *Hybrid constructed wetlands for the National Parks - a case study, requirements, dimensioning, preliminary results*. In: Natural and Constructed Wetlands. Nutrients, heavy metals and energy cycling, and flow. Springer International Publishing Switzerland, Vymazal, J. (Eds.), 247-265.
- Masi, F., Martinuzzi, N., Bresciani, R., Giovannelli, L. & Conte, G. 2007. Tolerance to hydraulic and organic load fluctuations in constructed wetlands. *Water Sci. Technol.* **56 (3)**, 39-48.
- Masi, F., Caffaz, S. & Ghrabi, A. 2013 Multi-stage constructed wetlands systems for municipal wastewater treatment, *Water Sci. Technol.* **67**, 1590–1598.
- Massoud, M. A., Tarhini, A. & Nasr, J. A. 2009 Decentralized approaches to wastewater treatment and management: Applicability in developing countries. *J. Environ. Manage.* **90 (1)**, 652–659.

- 1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
- Nastawny, M. & Jucherski, A. 2013 Assessing technical reliability of an on-site sewage treatment plant with filtration bed system, by using modified Weibull's method. *Probl. Inż. Rol.* **2 (80)**, 165–175 (in Polish).
- Niku, S., Schroeder, E.D. & Haugh, R.S. 1982 Reliability and stability of trickling filter processes. *J. Water Pollut. Control. Fed.* **54 (2)**, 129–134.
- Oliveira, S. C. & Sterling, M. V. 2008 Reliability analysis of wastewater treatment plants. *Water Res.* **42**, 1182–1194.
- Osaliya, R., Kansime, F. Oryem-Origa, H. & Kateyo, E. 2011 The potential use of storm water and effluent from a constructed wetland for re-vegetating a degraded pyrite trail in Queen Elizabeth National Park, Uganda. *Physics and Chemistry of the Earth, Parts A/B/C* **36 (14-15)**, 842-852.
- Platzer, C. & Mauch, K. 1997 Soil clogging in vertical flow reed beds - mechanisms, parameters, consequences and.....solutions? *Water Sci. Technol.* **35 (5)**, 175–181.
- Regulation of the Minister of Environment on 24.07.2014. On the conditions to be met when sewage into water or soil and on substances particularly harmful to the aquatic environment, Dz. U. nr 239 poz. 1800 (in Polish).
- Sanchez-Ramos, D., Sánchez-Emeterio, G. & Beltrán, M. F. 2015 Changes in water quality of treated sewage effluents by their receiving environments in Tablas de Daimiel National Park, Spain. *Environ. Sci. Pollut. Res.* **23 (7)**, 6082-6090.
- Wałęga, A. 2009 Assessment of the wastewater treatment plants statistical methods. *Forum eksploatacja* **5 (44)**, 30–34 (in Polish).
- Wałęga, A., Miernik, W. & Kozień, T. 2008 The efficiency of a domestic sewage treatment plant type RetroFAST. *Przemysł Chemiczny* **87 (5)**, 210–212 (in Polish).
- Wojciechowska, E., Gajewska, M. & Ostojki, A. 2016. Reliability of nitrogen removal processes in multistage treatment wetlands receiving high-strength wastewater, *Ecol. Eng.* **98**, 365-371.