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# Impact of strontium non-stoichiometry of $\text{Sr}_x\text{Ti}_{0.3}\text{Fe}_{0.7}\text{O}_{3-\delta}$ on structural, electrical, and electrochemical properties for potential oxygen electrode of intermediate temperature solid oxide cells

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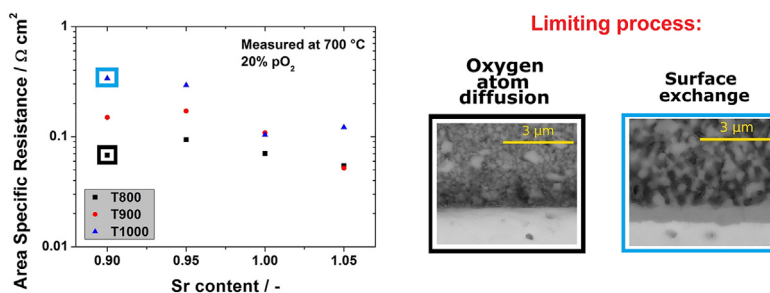
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## HIGHLIGHTS

- Knowledge about the influence of A site non-stoichiometry in STF has been extended.
- The electrochemical characterisation was performed on symmetrical and full cells.
- The DRT technique allowed to distinguish the dominant electrochemical process.
- The non-stoichiometric STF shows improved electrochemical properties.

## GRAPHICAL ABSTRACT



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## ABSTRACT

This work presents the results of a comprehensive study on the impact of the A-site non-stoichiometry of  $\text{Sr}_x\text{Ti}_{0.3}\text{Fe}_{0.7}\text{O}_{3-\delta}$  ( $x = 0.90, 0.95, 1.00, 1.05$ ) ceramics on their physico-chemical properties. The materials were fabricated by the conventional solid-state reaction method and their structure was determined by X-ray diffractometry, X-ray photoelectron spectroscopy and electron microscopy. Their sintering and thermal expansion properties were then evaluated. The electrical properties of the materials were determined by electrical conductivity and electrical relaxation measurements (on bulk materials) and by

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electrochemical impedance spectroscopy (EIS) studies of symmetrical, CGO-electrolyte based, porous electrodes. Finally, fuel cell tests with the non-stoichiometric electrodes were evaluated. To elucidate the electrochemical reaction pathways for oxygen reduction/evolution reaction, EIS measurements were carried out in different  $pO_2$  and were analysed via the distribution of relaxation times method. The results showed a dependence of materials' properties on the A-site non-stoichiometry, which can be used to fine-tune their properties, e.g. increase the surface exchange rate or decrease the thermal expansion coefficient.

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## Introduction

Solid Oxide Cells (SOCs) are energy conversion devices that can be used for energy generation (SOFCs – Solid Oxide Fuel Cells) and storage (by utilising SOECs – Solid Oxide Electrolysis Cells) [1]. Unfortunately, the performance of SOC is limited by the electrochemical reactions at the electrodes [2–4], including the oxygen reduction/evolution reaction rate at intermediate temperatures (<700 °C) [5–7]. Therefore, improved and new electrode materials are sought [8–14]. Perovskite oxides (general formula  $ABO_3$ ) with mixed ionic and electronic conductivity (MIEC) are perspective materials for SOFC electrodes [15–21], which allow for a wide range of compositional tailoring and fine-tuning of their structural and chemical properties. Historically, the most active oxygen electrodes contain Co, which provides high electrochemical activity due to its mixed valence [22–27]. Recent years have however highlighted Co as a problematic material due to its cost and unsustainable mining. Doped strontium titanates seem an interesting Co-free alternative material [28–30]. Doped strontium titanates have been used as oxygen membranes [31,32], resistive random access memory [33], oxygen sensors [34,35], coatings for porous stainless steel [36], fast electronic devices [37,38], quantum devices [39], and electrodes in SOFCs [40–43].

Previous research on the oxygen reduction reaction (ORR) on doped  $SrTiO_3$  has focussed on materials with substitution at the A or/and B sublattices [44–49]. For example, Zhang et al. reported excellent electrochemical properties at 700 °C (polarisation resistance  $0.043 \Omega \text{ cm}^2$ ) for  $SrTiO_3$  substituted at both sublattices, despite much lower electrical conductivity than the conductivity of  $La_{0.6}Sr_{0.4}Co_{0.2}Fe_{0.8}O_{3-\delta}$  ( $\sim 20 \text{ S cm}^{-1}$  and  $\sim 300 \text{ S cm}^{-1}$ , respectively) [43,50].

One of the options for improving perovskite materials is increasing the oxygen vacancies by introducing a non-stoichiometry at the A or B site [51–54]. Several works studying the influence of A-site or B-site deficiency on the properties of doped strontium titanate oxygen electrodes have been published. Ni et al. [55,56] investigated  $Sr_{1-x}Ti_{0.3}Fe_{0.6}Ni_{0.1}O_3$  ( $x = 0, 0.02, 0.05$ ) as an oxygen electrode at 750 °C. They have indicated that Sr deficiency promotes better electrochemical properties because of a higher amount of oxygen vacancies and a smaller thermal expansion coefficient (TEC). The best results in terms of electrochemical performance were obtained for the material with  $x = 0.05$  despite a

slight decrease of conductivity. Further research was carried out by Ni et al. [17], who improved the electrochemical properties of  $Sr_{0.95}Ti_{0.3}Fe_{0.6}Ni_{0.1}O_3$  by exsolution of (Ni,Fe)O nanoparticles. Zhu et al. proved that the exsolved  $Sr_{0.95}(Ti_{0.3}Fe_{0.63}Ni_{0.07})O_{3-\delta}$  anode has better electrochemical performance than stoichiometric material in the range 700 °C–850 °C. Shan and Guo's [57] research on a  $(Y_{0.08}Sr_{0.92})_{1-x}Ti_{0.6}Fe_{0.4}O_{3-\delta}$  mixed conductor showed a decrease in conductivity when the A-site deficiency increased. Similar behaviour of conductivity was reported for  $Sr_{1-x}Fe_{0.8}Ti_{0.2}O_{3-\delta}$  by Kharton et al. [58] and for  $Sr_xFe_{0.7}Ti_{0.3}O_{3-\delta}$  by Yang et al. [59]. Opposite behaviour of conductivity was observed by Li et al. for  $Sr(Ti_{0.6}Fe_{0.4})_{1-x}O_{3-\delta}$  where B-site deficiency was implemented [60]. Despite the above-mentioned literature reports on non-stoichiometric doped strontium titanates, the influence of the physical and chemical properties of non-stoichiometric materials on the electrochemical performance and electrochemical processes has not been shown.

In our previous work we have identified  $SrFe_{0.7}Ti_{0.3}O_{3-\delta}$  as an active catalyst [61]. Therefore, in this work we study of  $Sr_xFe_{0.7}Ti_{0.3}O_{3-\delta}$  (STF-x) with  $x = 0.90; 0.95; 1.00; 1.05$ . We report the fundamental material analysis including X-ray diffraction (XRD), particle size distribution (PSD), powder specific surface area (SSA), thermogravimetric analysis (TGA), linear thermal expansion, X-ray photoelectron spectroscopy (XPS),  $H_2$ -Thermally Programmed Reduction/Desorption ( $H_2$ -TPR/TPD) of STF-x powder and the results of total electrical conductivity and conductivity relaxation of STF-x pellets. Finally, an electrochemical impedance spectroscopy (EIS) study, including a distribution of relaxation times (DRT) analysis, of symmetrical cells under SOC operating conditions and different oxygen partial pressures are demonstrated.

## Experimental

### Materials synthesis

Stoichiometric  $Sr_{1.00}Ti_{0.3}Fe_{0.7}O_{3-\delta}$  (STF-100) and non-stoichiometric  $Sr_{0.90}Ti_{0.3}Fe_{0.7}O_{3-\delta}$  (STF-90),  $Sr_{0.95}Ti_{0.3}Fe_{0.7}O_{3-\delta}$  (STF-95), and  $Sr_{1.05}Ti_{0.3}Fe_{0.7}O_{3-\delta}$  (STF-105) powders were synthesised using the conventional solid state reaction method. Starting reagents:  $SrCO_3$  (EuroChem, Poland),  $TiO_2$  (EuroChem, Poland) and  $Fe_2O_3$  (Chempur, Poland) were mixed in a planetary ball mill (Fritsch, Pulverisette 7) for 12 h. All starting powders were >99.9% pure. The mixed reagent

powders of STF-100 and STF-105 (in the form of pellets) were sintered two times at 1200 °C (for 15 h each time) with an intermediate grinding step between the sinterings. Due to the higher sinterability of strontium-deficient compounds, the synthesis temperature was decreased to 1100 °C for the STF-90 and STF-95. After sintering, STF-x pellets were reground in a mortar and milled in two stages in a planetary ball mill. Firstly, using 3 mm YSZ balls and a rotational speed of 1000 rpm for 1 h and next using 1 mm ZrO<sub>2</sub> balls and 1100 rpm, also for 1 h. Finally, the milled STF-x powders were thermally relaxed at 600 °C as described earlier [62].

### Sample preparations

For the electrical conductivity and electrical conductivity relaxation measurements, the synthesised STF-x powders were uniaxially pressed and sintered for 2 h at the same temperature as during synthesis. The achieved pellets were ~1 mm in thickness and ~12 mm in diameter. For the electrical conductivity relaxation studies, pellets were also cut into the shapes of a prisms (12 × 1 mm × 2 mm) using a precision tungsten wire saw.

Porous STF-x electrodes for electrochemical impedance spectroscopy of symmetrical cells were applied on a dense gadolinium-doped ceria (CGO-20, Ce<sub>0.8</sub>Gd<sub>0.2</sub>O<sub>2-δ</sub>) substrate. Commercially available CGO-20 (DKK, Japan) powders were pressed into pellets and sintered at 1400 °C for 8 h. The sintered disks had a diameter of 13 mm and 98% theoretical density. The CGO-20 pellets were polished down to a 3 μm finish and a thickness of 0.6 mm ± 10%. For the application of the STF-x materials on the CGO-20 substrates, the synthesised powders were mixed with a commercial vehicle (Heraeus, V-006 A) at a weight ratio of 2:3 using a planetary ball mill. The STF-x pastes were screen-printed on two sides of the CGO-20. Each side received two layers with a drying step at 130 °C after each application. Symmetrical samples were sintered at 800 °C, 900 °C and 1000 °C for 2 h under an air atmosphere. The produced electrodes had an active surface area equal to 0.5 cm<sup>2</sup> and ~20 μm thickness. As in our previous work, platinum was used as a current collector [61].

For application tests in a SOFC system, selected STF-x (x = 0.95 and 1.05) materials were also screen printed on commercial Elcogen button half cells (ACS-400B) and sintered at 800 °C and 1000 °C, respectively. Finally, for comparison, a reference SOFC with commercially available, state-of-the-art LSCF cathode material (ESL Europe) was sintered at 1050 °C (for 2 h).

### Material characterisations

The phase composition of the STF-x powders was characterised by the X-ray diffraction (XRD) technique. Measurements were carried out at room temperature in air using a Bruker D2 Phaser with an XE-T detector equipped with a Cu X-ray anode.

X-ray Photoelectron Spectroscopy analysis (XPS) was performed using an Omicron NanoTechnology X-ray photoelectron spectrometer with a 128-channel collector. The XPS measurements were performed under ultra-high vacuum conditions. Photoelectrons were excited by an Mg-

Kα X-ray source with an X-ray anode operated at 15 keV and 300 W. The spectra were deconvoluted using the XPSPEAK software.

The H<sub>2</sub>-TPR (temperature programmed reduction) was performed using an apparatus equipped with a TCD detector (Buck Scientific, USA), cold trap, and heated gas transfer line. 100 mg of sample powder was placed in a quartz reactor with an internal measurements of the bed temperature. The STF-x powders were degassed at 200 °C for 20 min in a stream of He prior to the measurements. The samples were reduced under the flow of a 40 ml min<sup>-1</sup> 5% H<sub>2</sub>/Ar gas mixture. The tests were performed up to 900 °C with a heating rate of 10 °C min<sup>-1</sup>.

O<sub>2</sub>-TPD (temperature programmed desorption) was performed using 250 mg of prepared powdered sample with the preparation step as described for the H<sub>2</sub>-TPR experiment. After the degassing step and cooling down to 50 °C, the quartz reactor was flushed with pure 4N5 O<sub>2</sub> (40 ml min<sup>-1</sup>) for 1 h. After that, the gas was switched back to He for 1 h in order to equilibrate. The O<sub>2</sub>-TPD was performed up to 900 °C with a heating rate of 10 °C min<sup>-1</sup>. The profiles were collected using the PeakSimple software with a resolution of 1 Hz.

The specific surface area (SSA) was measured and calculated according to the BET isotherm model using a NovaTouch LX1 physisorption apparatus (Quantachrome, USA). The powder samples were degassed at 300 °C for 3 h under a vacuum prior to the measurement.

The particle size distributions of the powders were obtained using a Zetasizer Nano dynamic light scattering analyser (Malvern Panalytica). Measurements of the STF-x solution in ethanol using backscattering mode (detection angle was 173°) were performed at room temperature after a 20 min ultrasound bath.

The kinetics of the thermal decomposition of the STF-x powders were evaluated using thermogravimetric analysis (TGA). The TGA experiments were carried out using a microbalance (CI Precision MK5) in the temperature range between 900 °C and 200 °C. During the whole measurement procedure, air was fed to the furnace chamber at a flow rate of 40 ml min<sup>-1</sup>. No baseline correction was made for the change in atmosphere density during heating.

Linear thermal expansion results for the STF-x powders were obtained with a Netzsch DIL 402. Pressed powers in form of cylinder were placed in measuring chamber. The samples were heated up to 1100 °C at a heating rate of 5 °C min<sup>-1</sup>, and after 15 min of dwelling, were cooled down to room temperature at the rate of 3 °C min<sup>-1</sup> (all in Synthetic Air).

### Electrical and electrochemical performance analysis

DC electrical conductivity measurements of the STF-x pellets between 900 °C and 200 °C, were performed using the van der Pauw technique, as described in previous work [61]. The pellets were ~12 mm in diameter and ~1 mm thick. The conductivity was measured in 20% O<sub>2</sub>, 5% O<sub>2</sub> and 1% O<sub>2</sub>. Synthetic air was used as the base gas, which was further diluted with 5 N Ar using Brooks thermal mass flow controllers to obtain lower pO<sub>2</sub>.

To specify the chemical oxygen surface exchange coefficient (k\*) and chemical diffusion coefficient of oxygen (D\*), the

electrical conductivity relaxation (ECR) technique was used [63]. Studies were performed in a small tube furnace (internal diameter ~20 mm) with 64 cm<sup>3</sup> gas volume. The applied temperatures were 800 °C, 750 °C, 700 °C, 650 °C, and 600 °C. During the four-point single frequency electrochemical impedance spectroscopy measurement (1 Hz), the oxygen partial pressures were changed from 20% O<sub>2</sub> to 10% O<sub>2</sub> and the reverse. The impedance was logged every 5 s until sample stabilisation. The gas flow was constant during the measurement (80 ml min<sup>-1</sup>). After converting the recorded impedance to conductivity ( $\sigma$ ), the results were analysed using the ECR-TOOLS software [64].

For electrochemical impedance spectroscopy (EIS) measurements, a Novocontrol Alpha-A with a ZG-4 interface was used. Symmetrical cells were tested in a 4-wire compression cell placed inside a sealed quartz tube. All measurements were at 25 mV amplitude with a frequency range varying from 3 MHz to 0.05 Hz. In the case of the STF-x electrodes sintered at different temperatures evaluated by impedance spectroscopy, each sample was measured in synthetic air between 800 °C and 500 °C. Samples for the selected sintering temperature were tested at 700 °C under a controlled oxygen concentration (100%, 50%, 20%, 10%, 5%, 2.5%, 1%). Appropriate gas mixtures were achieved using a Brooks thermal mass flow controller.

Characterisation of the fuel cells was performed on an Open Flanges™ test setup by Fiaxell. The anode of the tested fuel cell was electrically connected by a nickel mesh. An Au mesh was used to connect the cathode side. A thin layer of LSC (Fiaxell ink paste) was brush painted on all cathodes (STF-x and LSCF) before the test and dried at 70 °C to improve current collection. Alumina felt was used to separate the gases. The Fiaxell setup was placed inside a Kitec temperature controller furnace. The fuel cells were heated up to 750 °C (3 °C min<sup>-1</sup>) for reduction and then cooled down to 700 °C for the main test after 24 h stabilisation. Reduction of the anode was conducted in H<sub>2</sub> with 3 vol% of steam, while on the cathode side, synthetic air was applied as the oxidant. Electrochemical impedance spectroscopy (at OCV and 3 vol% of steam) and current–voltage plots were measured by a Solartron 1260/1287 frequency analyser. EIS tests with a controlled oxygen concentration (3%, 5%, 10%, 20%, 50%) were performed with 50 vol% of steam. Appropriate oxygen concentration (cathode side) and steam content (anode side) were achieved using a Brooks thermal mass flow controller. High steam content was obtained by mixing hydrogen and oxygen in an external tubular furnace (700 °C) containing a platinum catalyst. All fuel cell tests were conducted with the total flow rates of 100 ml min<sup>-1</sup> and 200 ml min<sup>-1</sup> on anode and cathode side, respectively.

In order to designate the Area Specific Resistance (ASR) collected EIS spectra (polarisation resistance) were recalculated for the area of the electrode (0.5 cm<sup>2</sup>) and divided by two as the interfaces were identical. Each impedance spectrum was corrected for the inductance of the rig. The data was analysed by the DRTTOOLS software [65] in the same manner as earlier [61]. In the case of tests with different oxygen concentrations, the data were also fitted using the Elchemea Analytical web-tool ([www.elchemea.com](http://www.elchemea.com), DTU Energy).

## Post-mortem SEM

Images of the polished cross sections (with a 1 μm finish) of the measured symmetrical cells with STF-x porous electrodes sintered at different temperatures and of dense STF-x pellets were taken by an FEI Quanta FEG 250 Scanning Electron Microscope (SEM) with a backscattered electron detector and 20 kV in high vacuum. Chemical composition of polished cross-section of STF-x pellets was determined using the Thermo Fischer Phenom XL microscope with an integrated energy dispersive x-ray spectrometer (EDX).

## Results and discussion

### Characterisation of Sr<sub>x</sub>Ti<sub>0.3</sub>Fe<sub>0.7</sub>O<sub>3-δ</sub> powders and bulk materials

The crystallographic structure of the prepared powders was characterised by X-ray diffractometry (XRD). All investigated Sr<sub>x</sub>Ti<sub>0.3</sub>Fe<sub>0.7</sub>O<sub>3-δ</sub> powders revealed a cubic perovskite structure (*Pm-3m*), i.e. the structure remained stable even though altering the A-site occupation. Fig. 1 A) shows that the measured XRD patterns match well with the SrTiO<sub>3</sub> cubic lattice obtained from the crystallographic database. What is more stoichiometry of obtained STF-x materials was confirmed by the EDX analysis of sintered pellets (Table S.1). A small peak on XRD patterns related to the SrCO<sub>3</sub> phase could be identified (at 2θ ~24°) for STF-100 and STF-105. Due to high reactivity of doped strontium titanates, on the surface of STF-100 and STF-105 small amount of SrCO<sub>3</sub> is forming via reaction of terminating SrO crystal planes with CO<sub>2</sub> from the air, what cannot be avoided during the powder preparation, processing, or storage [66]. The presence of the SrCO<sub>3</sub> compound is of no surprise and can be easily explained on the basis of the research on the SrO–CO<sub>2</sub>–SrCO<sub>3</sub> equilibrium system, where the process of the carbonate formation greatly depends on the partial pressure of the CO<sub>2</sub> and the humidity of the atmosphere under which the powder was prepared. Above 900 °C the SrCO<sub>3</sub> is favoured to be decomposed into SrO what was confirmed by firing powders at 950 °C for 24 h in synthetic air (Figure S.2). This indicates that under the working conditions of the cell, where there is no obvious availability of the CO<sub>2</sub> in the gas stream, the surficial SrCO<sub>3</sub> is most likely being decomposed nearly fully into SrO [67–69].

The unit cell parameters were calculated each time using Rietveld refining method (GOF <1.8) and plotted as a function of the Sr-content in Fig. 1 B). The unit cell size of the stoichiometric STF-100 was 3.8845 (5) Å, which is in very good agreement with the literature data [28,70]. For the STF-90, STF-95 and STF-105 unit cell size equals to 3.8909 (1) Å, 3.8879 (2) Å and 3.8832 (7) Å, respectively. A good, monotonic correlation between the A-site occupation and the unit cell size is observed. Small deviation from linear trend probably is correlated with SrCO<sub>3</sub> formation in case of STF-105. Removal of Sr from the STF results in an increasing unit cell size. Sr<sup>2+</sup> deficiency can be charge-balanced by the removal of oxygen (O<sup>2-</sup>) from the lattice (the formation of oxygen vacancies) or via oxidation of iron ions. Such a mechanism was observed i.a. by Zhao et al. [71] in yttrium-doped strontium titanate with A-

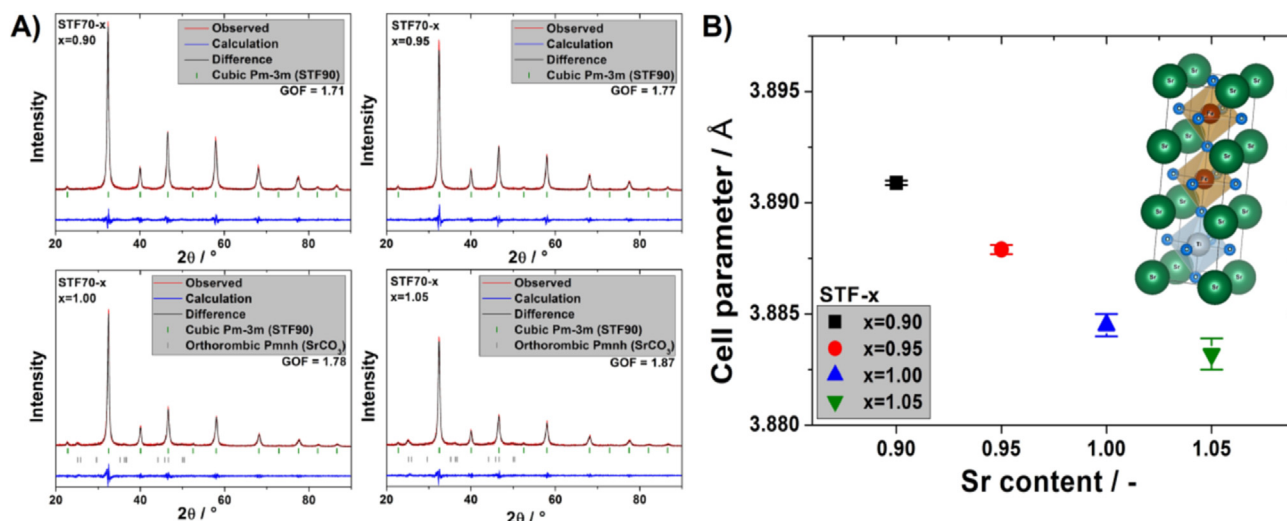


Fig. 1 – X-ray diffractometry spectra of the STF-x powders measured at room temperature (A) and calculated cell parameter value (B).

site deficiency ( $(Y_{0.08}Sr_{0.92})_{1-x}TiO_{3-\delta}$ ). Strontium deficiency in the structure was charge-compensated by both the decrease of  $Ti^{3+}$  ion concentration and the increase of oxygen vacancy concentration. In this work, change of the valence state of iron from 3+ to 4+ induces a large decrease (about 10%) of the ionic radius (0.645 Å vs. 0.585 Å) [72], whereas the observed lattice size change (STF105 vs STF90) is opposite (increase about ~0.2% of the unit cell parameter). Thus the effect of Sr-nonstoichiometry on the lattice must be complex and involve these two compensation mechanisms.

Moreover, the removal of oxygen from the structure and the change in the oxidation state of iron also change the length of the bonds between Fe and O in  $TiO_6$  octahedra. This, in turn, significantly affects the unit cell parameter what was

observed in this work. Ward et al. shows that for  $Pr_{1-x}Sr_xFeO_{3-\delta}$  with lowering concentration of  $Sr^{2+}$  unit cell parameter also increase and with the increase of the oxidation state of iron (smaller ionic radius), Fe–O inter-ion distance leads to lowering of the average Fe–O bonding energy of the redox-active Fe [73]. All facts mentioned above may explain the observed changes in the lattice constant with the changing content of strontium in the structure.

The morphology of the powders was characterised by scanning electron microscopy and particle size measurements, supplemented with specific surface area (SSA) determination.

Fig. 2 A) presents the results of the particle size distribution (PSD) measurements and specific surface area of the STF-x

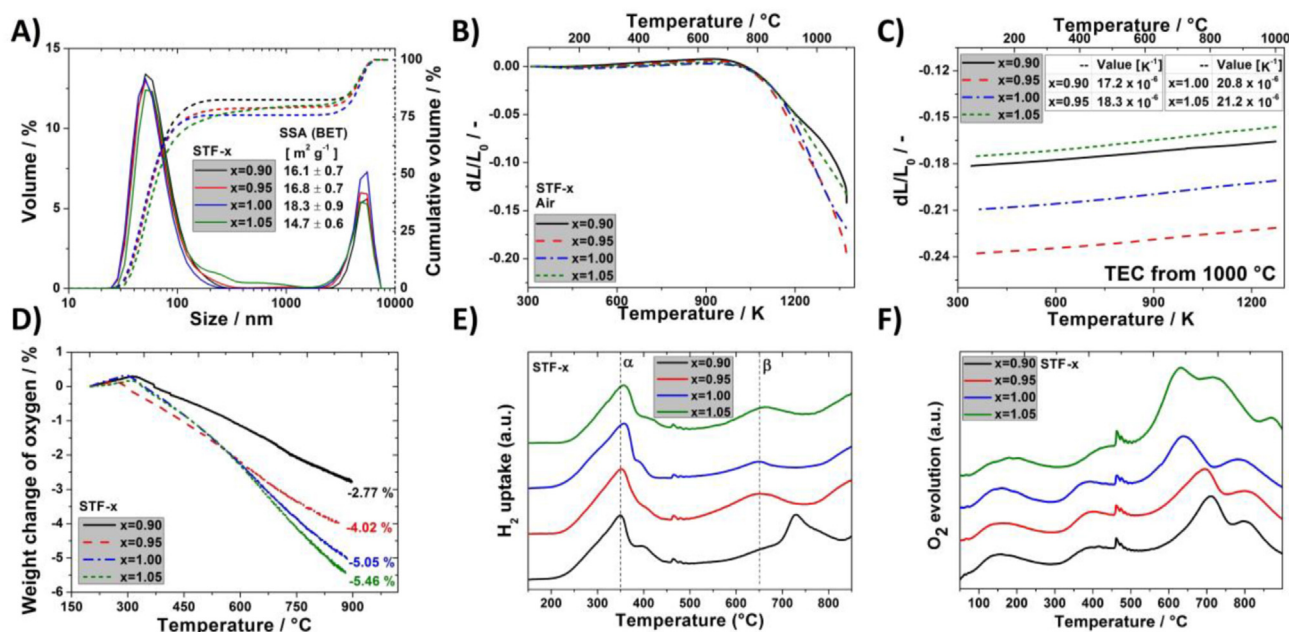


Fig. 2 – Particle size distribution and specific surface area (A), sintering/expansion curves (B–C), thermogravimetric dependence (D), H<sub>2</sub>-TPR (E) and O<sub>2</sub>-TPD (F) curves for investigated STF-x.

powders. For all cases, similar particle size distributions and specific surface areas ( $\sim 15 \text{ m}^2 \text{ g}^{-1}$ ) were observed, i.e. no clear effect of the A-site occupation on the powders (e.g. particle coarsening, etc.) could be identified. Approximately 75% of the cumulative volume was formed by particles smaller than 100 nm. PSD measurement showed that  $\sim 25\%$  of the cumulative volume was formed by larger particles ( $\sim 5 \mu\text{m}$ ), whilst the SEM examination (Figure S.1) confirmed presence of only relatively small particles. Interestingly, there was no large aggregates found during the SEM imaging, what may suggest that the presence of the larger particles in PSD result may be caused by the apparatus error due to the upper detection limit. The obtained particle size of the powders can be considered small, which may be advantageous for electrochemical reaction for mixed conducting SOC electrodes. For comparison, Schulze-Koppers et al. reported preparation of  $\text{SrTi}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  materials also including ball milling. In their case, 90% of the particles had a size lower than a few microns with a resulting much smaller specific surface area ( $\sim 3 \text{ m}^2 \text{ g}^{-1}$ ) [74].

The results of the dilatometry measurements conducted in air are presented in Fig. 2 B)–C). The sintering profile for all STF-x materials looks similar to that reported earlier for the  $\text{SrTi}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  materials [62]. For all of the investigated compounds, the onset of sintering is quite similar: from  $\sim 760^\circ\text{C}$  to  $\sim 810^\circ\text{C}$ . The main differences are observed during heating between  $800^\circ\text{C}$  and  $1100^\circ\text{C}$ . The most Sr-deficient sample, STF-90, shows non-linear behaviour at high temperatures, whereas the STF-95 and STF-100 show similar sintering profiles.

The TEC values for the STF-x were calculated based on the cooling profiles from dilatometry. Obtained values were  $\sim 17$ ,  $\sim 18$ – $21$ , and  $\sim 21 \times 10^{-6} \text{ K}^{-1}$  for STF-90, STF-95, STF-100, and STF-105, respectively. The differences between the TEC values indicate that the STF-x thermal expansion properties are directly related to the strontium content, possibly caused by different chemical expansion contributions due to oxygen release and different amounts of reducible  $\text{Fe}^{4+}$  ions, which is consistent with the oxygen loss data (Fig. 2 D). The introduction of Sr-nonstoichiometry can be used to reduce the relatively high TEC value of STF-x. Kharton et al. showed comparable TEC values for  $\text{Sr}_{0.97}\text{Ti}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$  where  $y > 0.6$  [15]. The values are also comparable with data from Zhang et al. although the TEC profiles reported here are linear in the measurement range RT– $900^\circ\text{C}$ , whereas they reported non-linear behaviour [40]. Despite this relatively high TEC value, the STF-x materials can be successfully used as a SOC oxygen electrode, as is in the case of the state-of-the-art materials, e.g.  $\text{La}_{0.6}\text{Sr}_{0.2}\text{Co}_{0.2}\text{Fe}_{0.8}\text{O}_{3-\delta}$  or  $\text{La}_{0.6}\text{Sr}_{0.4}\text{CoO}_{3-\delta}$ , with  $\text{TECs} > 18 \times 10^{-6} \text{ K}^{-1}$  [75,76].

To study the temperature-dependent weight loss properties due to oxygen release caused by the thermal reduction of transition metals, thermogravimetric (TG) measurements were carried out between  $200^\circ\text{C}$  and  $900^\circ\text{C}$  in air. Since the changes in powders' mass during TG measurements were related only to the absorption or release of the oxygen, Fig. 2 D) shows only the change of the mass of oxygen contained within the STF-x compounds as a function of temperature. All samples show weight loss on heating, indicative of lattice oxygen release and the formation of oxygen vacancies. Up to  $550^\circ\text{C}$ , the weight loss followed a similar trend for STF-95/100/

105, whereas for the STF-90 sample, smaller weight loss was observed. Above  $550^\circ\text{C}$ , after reaching  $900^\circ\text{C}$ , the weight loss was the highest ( $>5\%$ ) for the samples with high Sr content (STF-105 and STF-100). The lowest weight loss was measured for the most Sr-deficient sample (STF-90:  $\sim 2.8\%$ ). The oxygen release accompanied by oxygen vacancy formation must be charge balanced to preserve electrical neutrality through the reduction of  $\text{Fe}^{4+}$  to  $\text{Fe}^{3+}$ .

The determined weight change, presented in Fig. 2 D), has a similar profile to that reported by Zhang et al. The main difference is the temperature of the inflection point. In this work, the inflection points occur at  $\sim 300^\circ\text{C}$ , while for  $\text{SrTi}_{1-y}\text{Fe}_y\text{O}_{3-\delta}$ , Zhang obtained the inflection at  $\sim 400^\circ\text{C}$  [40].

The  $\text{H}_2$ -TPR profiles of the STF-x samples are presented in Fig. 2 E). The reduction profiles in all cases contain two main peaks located at around  $350^\circ\text{C}$  ( $\alpha$ ) and  $650^\circ\text{C}$  ( $\beta$ ) except for the STF-90 sample where the secondary  $\beta$  peak is shifted  $100^\circ\text{C}$  towards higher temperatures. Sr and Ti are assumed not to undergo reduction under the used conditions, so the peaks were assigned to Fe-related processes only. The  $\alpha$  peak was associated with the reduction of  $\text{Fe}^{4+}$  to  $\text{Fe}^{3+}$ , while the  $\beta$  peak located at higher temperatures was related to the reduction of  $\text{Fe}^{3+}$  to  $\text{Fe}^{2+}$ . The additional peak at  $\sim 720^\circ\text{C}$ , visible for the STF-90 sample, could be attributed to the simultaneous reduction of created  $\text{Fe}^{2+}$  to  $\text{Fe}^0$  [77,78]. The existence of metallic  $\text{Fe}^0$  in the STF-90 compared to the other compounds was also confirmed through the post-mortem XRD measurements (Figure S.3).

The  $\alpha$  peak shifts slightly to a higher temperature with the increasing amount of Sr in the A sublattice. Higher amounts of Sr in the lattice stabilise the STF structure, increasing its reduction temperature presenting also an increase in the concentration of lower valence iron ions.

The oxygen desorption measurements ( $\text{O}_2$ -TPD) revealed quite similar behaviour of the STF-x samples at low temperatures up to  $\sim 550^\circ\text{C}$ , which can be described by the release of chemisorbed oxygen molecules bound loosely to the sorption centres at the surface of the powders (Fig. 2 F). At high temperatures, the peaks were correlated to the evolution of the bulk lattice oxygen [35]. The STF-100 and STF-105 showed faster onset with the peak position of  $640^\circ\text{C}$ , whereas for the STF-95 and STF-90 the peaks were shifted to  $700^\circ\text{C}$  and  $710^\circ\text{C}$ , respectively. The changed look of the  $\text{O}_2$ -TPD profile of STF-105 sample in the high temperature region most probably corresponds to the evolution of the  $\text{CO}_2$  gas from the  $\text{SrCO}_3$  secondary phase.  $\text{O}_2$ -TPD measurements indicate that Sr-deficiency results in a lower tendency of the perovskite to release the oxygen from its structure, which is consistent with the TG results, where the Sr-deficient samples showed decreased thermal reducibility.

The surface composition of the STF-x powders was measured using XPS at room temperature under ultra-high vacuum conditions. Deconvolutions of the  $\text{Fe}2p$  spectra for all samples are presented in Fig. 3 A). Both  $\text{Fe}^{3+}$  and  $\text{Fe}^{4+}$  species were identified in all of the synthesised materials. The doublet peak separated by  $134 \text{ eV}$  located at around  $710 \text{ eV}$  was assigned to the  $\text{Fe}^{3+}$  state of iron, whilst the peak situated at  $\sim 712.5 \text{ eV}$  corresponded to the coexisting  $\text{Fe}^{4+}$  ions. This behaviour is very characteristic for this type of the compounds based on the Fe-substituted  $\text{SrTiO}_3$  [55,79]. The

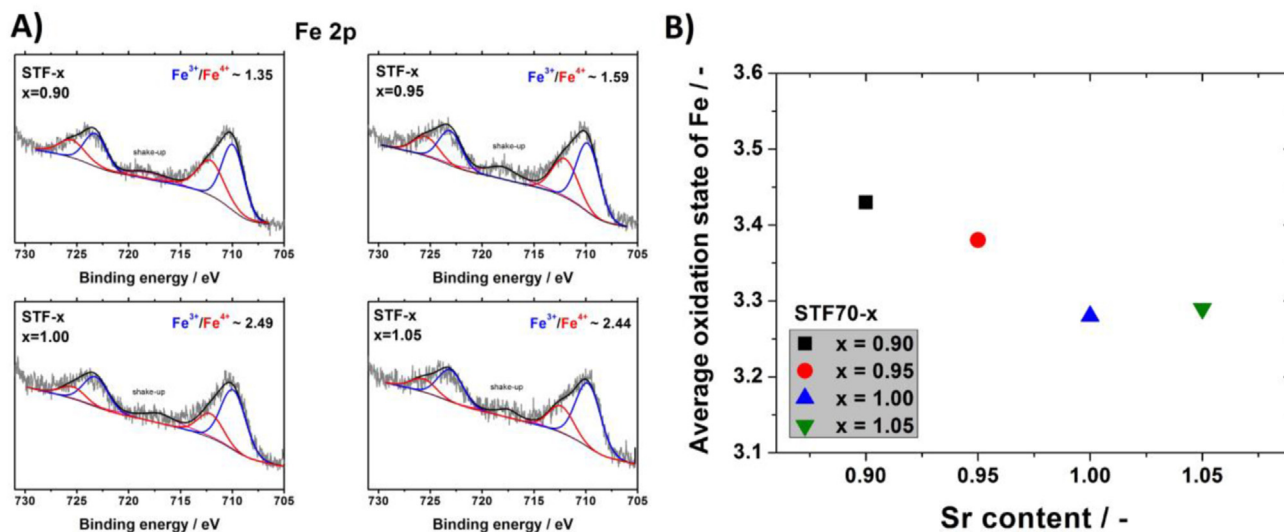


Fig. 3 – Fe 2p spectra (A) and relation of  $\text{Fe}^{3+}/\text{Fe}^{4+}$  ions as a function of Sr content for STF-x powders.

characteristic shake-up lines were also detected, clearly distinguishable mainly for STF-90 and STF-95. It is visible that with the increasing strontium content in the A sublattice, the  $\text{Fe}^{3+}/\text{Fe}^{4+}$  ratio is being elevated. The increase in the Fe mean valence (Fig. 3 B) is considered as one of the mechanism of the charge compensation when A site is being depleted of Sr ions. Despite that the oxygen nonstoichiometry and formation of the oxygen vacancies may have the dominant role, due to the relatively low changes in the increase of the amount of higher valence Fe ions comparing to the removal of the A site cations. Even though the XPS technique surveys just a surface of the materials we can, with high dose of the probability, estimate that similar stoichiometry between  $\text{Fe}^{3+}$  and  $\text{Fe}^{4+}$  state is being maintained throughout the material bulk, if the compound is single-phase. It is also proven when looking at the complementary results of the more bulk-related techniques like the temperature-driven oxygen loss ( $\text{O}_2$ -TPD) and TEC measurements revealing the changes in the Fe oxidation state.

In the case of the Sr3d spectra (Figure S.4), three Sr states were distinguished and associated with the Sr contained within STF-x structure, SrO and  $\text{SrCO}_3$  (with a characteristic peak at 289.5 eV in C1s spectra) [80–82]. Increasing the Sr content at A sublattice lead to decrease in the relative share of Sr forming the STF-x and increased its participation in the surficial formation of the SrO and, after reacting with atmospheric  $\text{CO}_2$ , the corresponding carbonate -  $\text{SrCO}_3$ . A superficial effect of the formation of  $\text{SrCO}_3$  by the exposure for  $\text{CO}_2$  was reported earlier and is closely related to the existence of surface SrO terminations in strontium titanates [40,66]. The presence of the  $\text{SrCO}_3$  was confirmed by the XRD measurement. Based on the XPS, the total surface composition was determined. The introduction of Sr-deficiency leads to lowering of the surface Sr segregation. For Sr-deficient materials, the estimated surficial Sr content vs. (Ti + Fe) content was ~1, what stands for the formation for the non-segregated material or high homogeneity (Figure S.5). At the same time for stoichiometric material, this value reached ~1.3 indicating slight segregation of the Sr towards the surface. For highly Sr

enriched materials, the surface Sr ratio peaked at the value of ~2 and thus indicated formation of the highly Sr surface-rich compound. Thus, one can correlate the Sr-stoichiometry in the lattice with the existence of the additional surface segregates of the Sr-base compounds.

After the deconvolution of the Ti2p spectra it was observed that titanium ions generally take up the  $\text{Ti}^{4+}$  valence (Fig. S.4). Each  $2p_{3/2}$  peak of Ti2p spectra was situated at ~457.8 eV with the separation energy of 5.8 eV for the doublet. It clearly correspond to the Fe-doped  $\text{SrTiO}_3$  lattice, what is in agreement with the previously obtained data by the research of Zhang S. L. et al. [43]. According to the studies on  $\text{SrTi}_{0.7}\text{Fe}_{0.3}\text{O}_3$  performed by Nanning A. et al. [83] using Near Ambient Pressure XPS (NAP-XPS) the location of the  $\text{Ti}2p_{3/2}$  peak depends on the surrounding atmosphere conditions. Under highly reducing conditions the peak is being shifted towards higher bonding energies of ~458.4 eV and while in oxidizing gases it is localized ~457.4 eV. Additionally, the  $\text{Ti}2p_{1/2}$  peak is broadened, what is a typical behaviour of this feature.

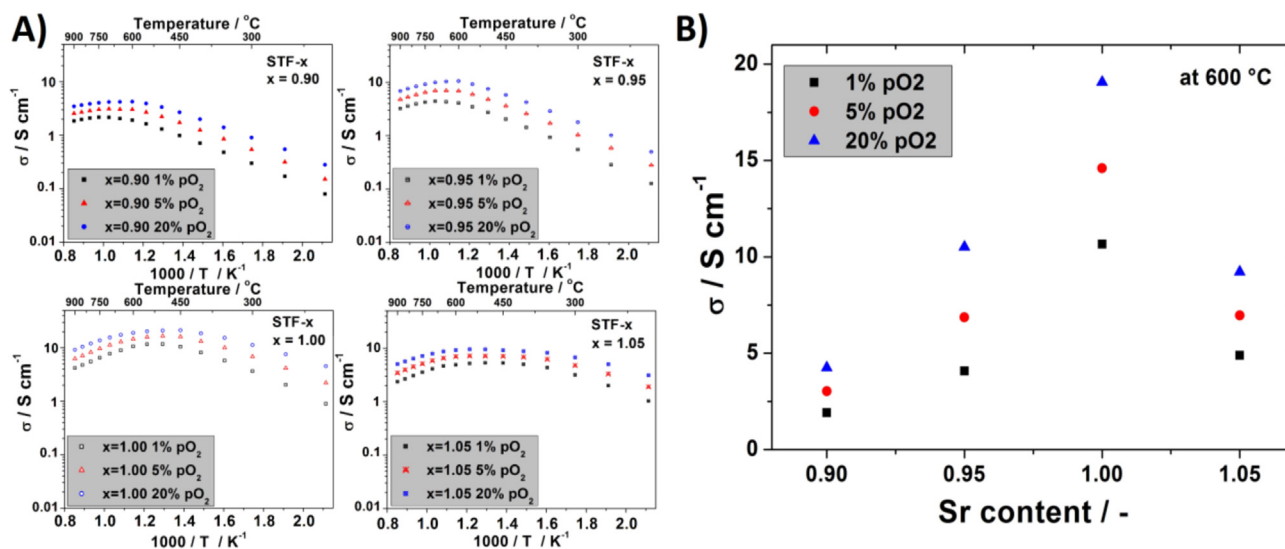
### Electrical properties

Total electrical conductivity was investigated as a function of temperature (from 900 °C to 200 °C) in different oxygen concentrations (1%, 5% and 20%). The results of the electrical measurements of the STF-x pellets are presented in Fig. 4 A).

According to the equation derived from the reaction of oxygen incorporation and mass action law [84] (Kröger–Vink notation), a concentration of electron holes can be expressed as:

$$p = \left( \frac{K}{[V_{\text{Sr}}]} \right)^{\frac{1}{2}} \times p\text{O}_2^{\frac{1}{4}} \quad (\text{equation 1})$$

where  $p$  denotes the concentration of electron holes,  $K$  denotes a chemical reaction constant,  $[V_{\text{Sr}}]$  is the concentration of strontium vacancies and  $p\text{O}_2$  is an oxygen partial pressure. Based on Equation (1), it can be stated that the concentration of electron-holes and thus the conductivity of all STF-x



**Fig. 4** – Electrical conductivity plots of sintered STF-x pellets measured at 20% O<sub>2</sub>, 5% O<sub>2</sub> and 1% O<sub>2</sub> (A) and relation of conductivity at 600 °C as a function of Sr content (B).

decrease with the decreasing oxygen partial pressure. This is in agreement with the experimental results for all investigated samples (see Fig. 4 A). The results of STF-90, STF-95 and STF-100 also indicate a decrease of the conductivity with the increasing strontium deficiency (Fig. 4 B) similar as in the literature [57,58] and in qualitative agreement with equation (1). At 600 °C at 20% oxygen concentration, the conductivity of the STF-90 was  $\sim 4$  S cm<sup>-1</sup>, whereas for STF-100 its value was  $\sim 18$  S cm<sup>-1</sup>, thus the effect of the Sr-nonstoichiometry is considerable. This behaviour is also in line with equation (1), which relates the concentration of electron-holes inversely to the concentration of strontium vacancies.

The results for STF-105 can be influenced by the sample porosity and presence of secondary phases. As presented in Figure S.6 in the Supplementary materials, the density of STF-90/95/100 was  $>94\%$ , whereas for the STF-105 the density was  $\sim 90\%$ .

The temperature for the maximum conductivity increases slightly for the materials with the higher strontium deficiency (for STF-90 and STF-95 it is  $\sim 600$  °C, and for STF-100 and STF-105 it is  $\sim 500$  °C). Ni et al. also reported a slight change of the maximum conductivity temperature, but for their non-stoichiometric Sr<sub>1-x</sub>Ti<sub>0.3</sub>Fe<sub>0.6</sub>Ni<sub>0.1</sub>O<sub>3- $\delta$</sub> , the maximum shift was 50 °C [55]. The shift might be correlated with the TG results and O<sub>2</sub>-TPD, where the samples with higher Sr-deficiency showed decreased oxygen loss and delayed lattice oxygen evolution and thus decreased formation of charge balancing p-type carriers.

The chemical oxygen surface exchange ( $k^*$ ) and chemical diffusion ( $D^*$ ) coefficients were measured by the electrical conductivity relaxation (ECR) method. Due to the high sample density requirement,  $D^*$  and  $k^*$  were determined for STF-90, STF-95 and STF-100. Due to the porosity of the pellets after sintering, the STF-105 sample was not measured by ECR. The typical normalised data as a function of time for STF-90 and STF-100 measured at 700 °C is presented in Fig. 5 A). The total relaxation time at 700 °C was about 3000 s. Qualitatively, for all samples a faster equilibration time occurred during oxygen

adsorption and incorporation (change from 10% pO<sub>2</sub> to 20% pO<sub>2</sub>) than during desorption of oxygen (change from 20% pO<sub>2</sub> to 10% pO<sub>2</sub>), which might indicate good performance of this material when used as an oxygen electrode in fuel cells.

The calculated values of chemical surface exchange coefficient  $k^*$  and chemical oxygen diffusion coefficient  $D^*$  are presented in Fig. 5 B)–C). At 700 °C, the values of  $k^*$  are  $\sim 10^{-4}$  cm s<sup>-1</sup> and  $D^*$  from  $10^{-5}$  to  $10^{-6}$  cm<sup>2</sup> s<sup>-1</sup>. The data is consistent with the values (from an ECR experiment) for STF50 reported by Schulze-Küppers [74]. Moreover, the chemical oxygen surface exchange coefficient of STF-x (at 800 °C) has a higher value than for the state-of-the-art La<sub>0.6</sub>Sr<sub>0.4</sub>Co<sub>0.2</sub>Fe<sub>0.8</sub>O<sub>3- $\delta$</sub>  ( $\sim 1.2 \times 10^{-4}$  cm s<sup>-1</sup>) [63].

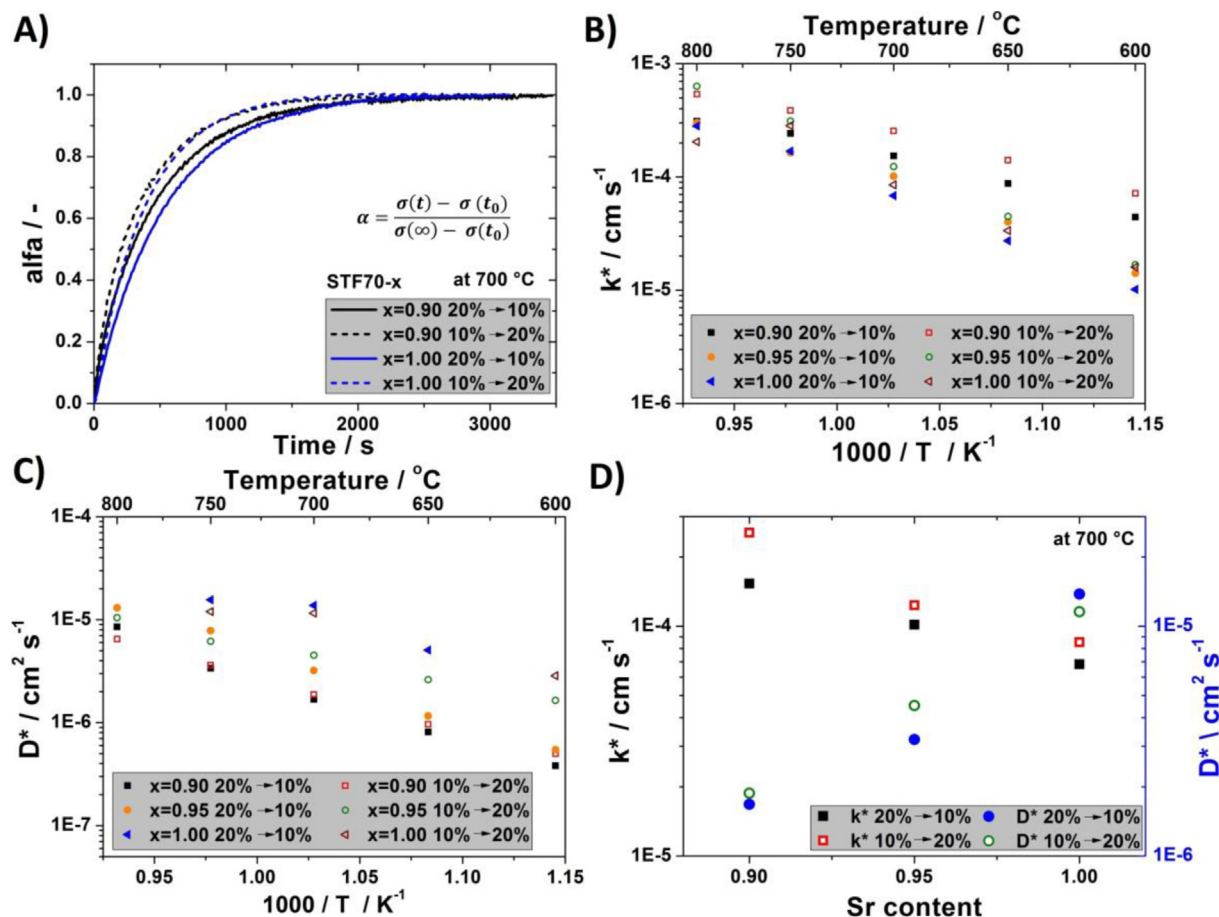
In this work,  $k^*$  at 800 °C for all STF-x ( $<9 \times 10^{-3}$  cm s<sup>-1</sup>) are one order of magnitude higher than the values obtained by Zhang et al. for SrTi<sub>0.3</sub>Fe<sub>0.7</sub>O<sub>3- $\delta$</sub>  ( $\sim 9 \times 10^{-4}$  cm s<sup>-1</sup>) [40], who, however, based their values on fitting of the electrochemical performance of the electrode to the Adler-Lane-Steele (ALS) model using detailed microstructural 3D analysis. This difference may be influenced by both other research methods for determining the value of  $k$  [44,85], as well as differences in the microstructure of the compounds [86] studied by Zhang et al. and in this work.

It was found that with an increasing strontium content,  $k^*$  decreases (Fig. 5 D), whereas  $D^*$  has the opposite trend. The calculated  $D^*$  ( $\sim 1 \times 10^{-5}$  cm<sup>2</sup> s<sup>-1</sup>) for STF-x at 800 °C is similar to those reported for the La<sub>0.6</sub>Sr<sub>0.4</sub>Co<sub>0.2</sub>Fe<sub>0.8</sub>O<sub>3- $\delta$</sub>  and SrTiO<sub>3</sub> materials [63,87]. In Fig. 5 D) shows the relation between the chemical oxygen diffusion coefficient and the Sr content (at 700 °C). According to equation (1), increasing the Sr content increases the concentration of electron-holes, which may increase the chemical oxygen diffusion coefficient  $D^*$ .

#### Electrochemical performance of Sr<sub>x</sub>Ti<sub>0.3</sub>Fe<sub>0.7</sub>O<sub>3- $\delta$</sub> oxygen electrodes

The results of EIS measurements and DRT analysis for symmetrical STF-x porous electrodes sintered at 800 °C, 900 °C and





**Fig. 5** – Exemplary normalised electrical conductivity relaxation plot of STF-x at 700 °C (A), calculated chemical oxygen surface exchange coefficient (B) and chemical oxygen diffusion coefficient (C) and relation between  $k^*$  and  $D^*$  as a function of Sr content at 700 °C.

1000 °C are presented in Fig. 6 A) and D); B) and E); C) and F), respectively.

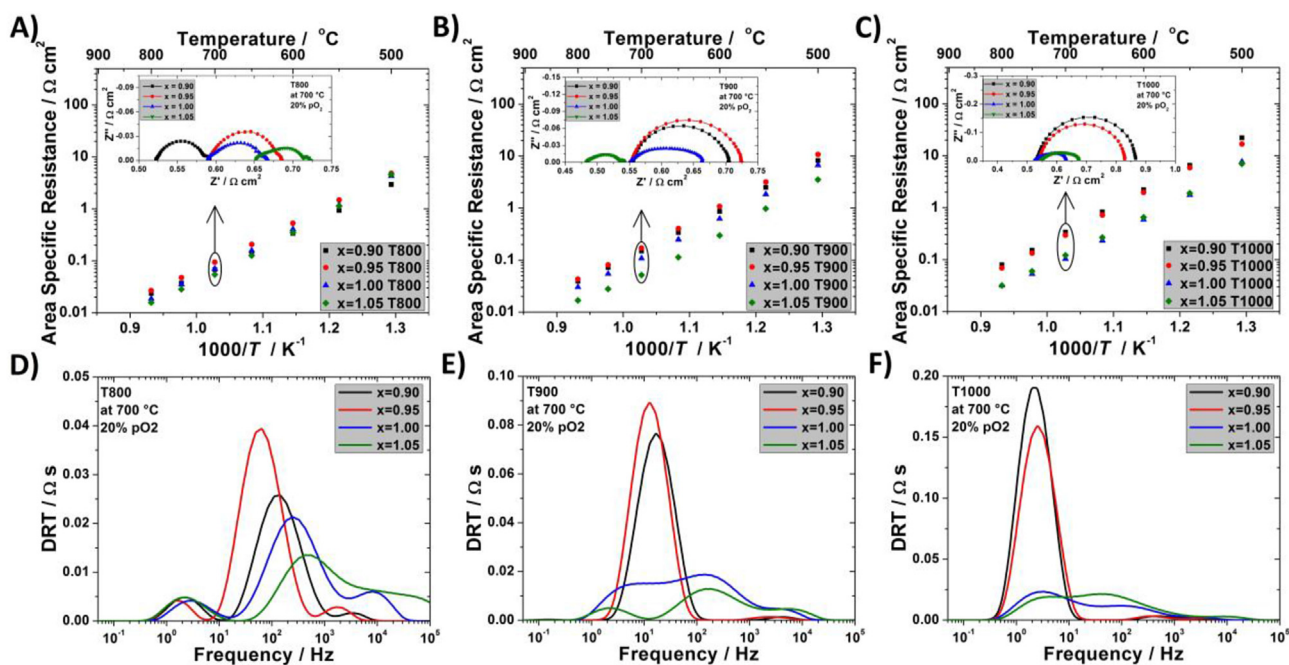
The STF-x materials showed overall high electrochemical activity for oxygen reduction/evolution reactions. For electrodes sintered at 800 °C, the Area Specific Resistance (ASR) values measured at 700 °C in air were all within the range of ~55–94  $\text{m}\Omega \text{cm}^2$ , and were lower than that reported for  $\text{SrTi}_{0.3}\text{Fe}_{0.7}\text{O}_{3-\delta}$  (112  $\text{m}\Omega \text{cm}^2$ ) [40] or  $\text{Sr}_{1-x}\text{Ti}_{0.3}\text{Fe}_{0.6}\text{Ni}_{0.1}\text{O}_{3-\delta}$  (~220  $\text{m}\Omega \text{cm}^2$ ) [55] obtained in similar conditions. The electrode performance below 150  $\text{m}\Omega \text{cm}^2$  is promising for high performance SOCs [88]. For the Co-containing  $\text{Sr}(\text{Ti}_{0.3}\text{Fe}_{0.7-x}\text{Co}_x)\text{O}_{3-\delta}$  reported by Zhang et al. ASR values of 40–90  $\text{m}\Omega \text{cm}^2$  were achieved [43]. For higher sintering temperatures, the Sr-deficient STF-90 and STF-95 show slightly worse performance than the STF-100 and STF-105. Interestingly, the highest performance among the tested electrodes was achieved for the STF-105 sintered at 900 °C. Even though the powder contained traces of strontium carbonate (detected by XRD) and the surface was enriched in strontium (detected by XPS), its ORR/OER performance was the highest, i.e. the polarisation resistance was the lowest (~55  $\text{m}\Omega \text{cm}^2$  at 700 °C). The specific reasons are not so obvious and are open to future research.

For the sintering temperature of 800 °C, the area specific resistance (ASR) values were comparable for all STF-x

electrodes, but as the sintering temperature increased, the differences in electrode performance also increased. The STF-90 was the most sensitive electrode to the effect of the sintering temperature, in contrast to the STF-105 (Figure S.7). For the sintering temperature of 1000 °C, the Sr-deficient compounds (STF-90 and STF-95) have almost twice the value of ASR in comparison to the STF-100 or STF-105. The change in electrochemical performance might come from the formation of a dense, interfacial layer, observed by SEM for STF-90 and STF-95 (Figure S.8). The high Sr content and its surface segregation hinders sintering of the electrodes and has a positive effect on the electrode performance.

The sintering temperature conditions for the preparation of the STF-90, STF-95 and STF-100 electrodes had no significant impact on the ohmic resistance (Figure S.9) as we reported earlier for  $\text{SrTi}_{0.3}\text{Fe}_{0.7}\text{O}_{3-\delta}$  [62]. The STF-105 slightly improved contact with the electrolyte with the increasing sintering temperature. Even though the electrical conductivity of the STF-x materials is quite low (1–20  $\text{S cm}^{-1}$  at 700 °C), this seems sufficient to provide good current collection in the measurements.

These results show, that the electrochemical performance of STF-x materials can be tuned by A-site non-stoichiometry and sintering conditions. The obtained ASR values are



**Fig. 6** – Impact of Sr non-stoichiometry on polarisation resistances of symmetrical cells with STF-x electrodes sintered at 800 °C, 900 °C and 1000 °C, respectively (A–C) and corresponding distribution of relaxation times results (D–F) for EIS spectra measured in 20% O<sub>2</sub> at 700 °C.

comparable to typical polarisation values reported for MIEC oxygen electrodes in the intermediate-temperature range [89,90], e.g. 0.1–1 Ωcm<sup>2</sup> at 600–700 °C.

#### Distribution of relaxation times analysis

The results of the DRT analysis (Fig. 6 D)–F) corresponding to the EIS spectra obtained at 700 °C in air (insets of Fig. 6 A)–C)) indicate differences in electrochemical processes depending on the Sr content.

For all STF-x sintered at the lowest temperature (800 °C), there are possibly two peaks related to two electrochemical processes, as also reported in our previous work for SrTi<sub>0.3</sub>Fe<sub>0.7</sub>O<sub>3-δ</sub> [61]. The low frequency peak (~1 Hz) is similar for all electrode materials and is most probably connected to gas diffusion within the porous electrodes. The main electrochemical process has a characteristic peak at the frequency of 30–300 Hz (middle frequency), depending on the compound. The lowest contribution and the highest characteristic frequency were obtained for STF-105. The contributions visible as higher frequency “shoulders” of lower magnitude might be indicative of Gerischer-type elements, typically considered for MIEC perovskite electrodes in this frequency range.

As the sintering temperature increased, the spectra changed shape. For the STF-90 and STF-95, only a single process became distinguishable in the DRT spectra (Fig. 6 E) and F)). The shape of the DRT spectrum for STF-100 and STF-105 seems to be insensitive to the sintering temperature and shows the gas diffusion and higher frequency contributions.

To evaluate the electrochemical processes for the STF-90 and STF-95 in more detail, the responses of the electrodes sintered at 900 °C were also investigated at 700 °C as a function of oxygen partial pressure (pO<sub>2</sub>). Fig. 7 A)–B) presents the selected EIS spectra and corresponding DRT spectra for the

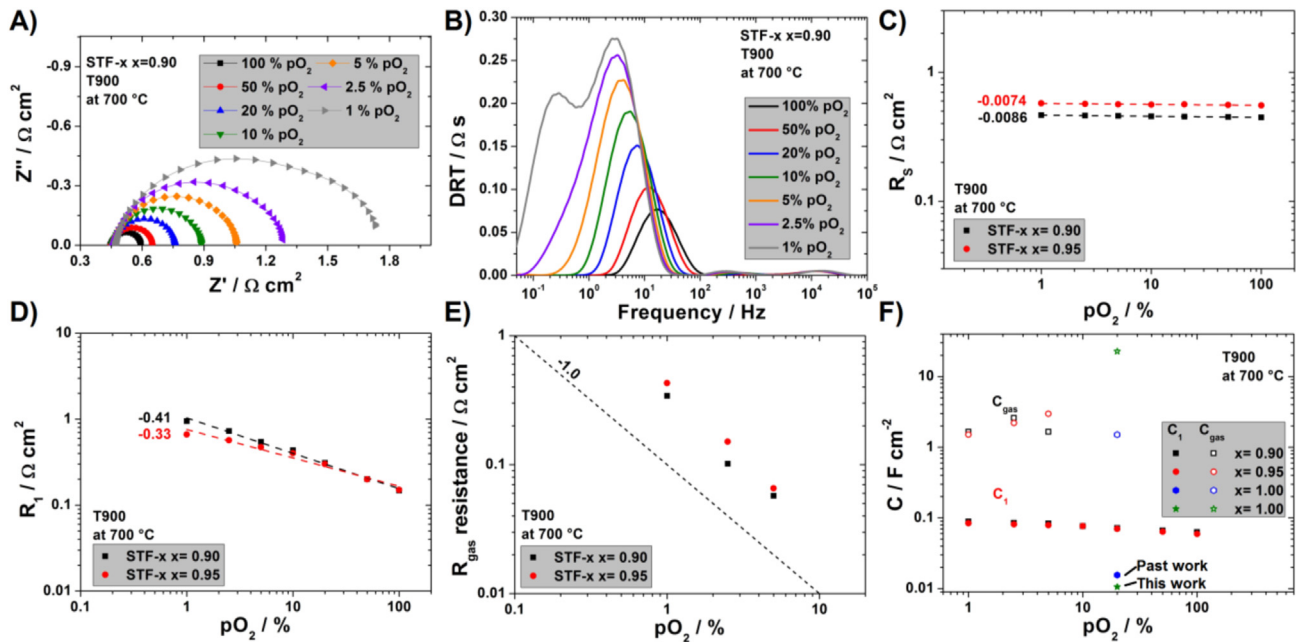
STF-90 at different oxygen concentrations. Similar results were achieved for the STF-95. The EIS measurement data were fitted by an equivalent circuit that consists of two R-CPE elements due to the occurrence of a low frequency contribution visible only at low pO<sub>2</sub> values (<5% O<sub>2</sub>).

The ohmic resistance (R<sub>s</sub>), low frequency resistance (R<sub>gas</sub>), middle frequency resistance (R<sub>1</sub>) and R-CPE calculated equivalent pseudo capacitances for the STF-90 and STF-95 as a function of oxygen partial pressure are presented in Fig. 7C)–F) and listed in Table S.2 and Table S.3. For pseudo capacitance calculation this formula was used:

$$C = \frac{(R^*Y)^{\frac{1}{n}}}{R} \quad (\text{equation 2})$$

where C is pseudo capacitance, R resistance of R-CPE element, Y capacitance of R-CPE element and n is dimensionless value. Additionally, for comparison, the results of the pseudo capacitance for the stoichiometric STF-100 at 20% pO<sub>2</sub>, reported earlier [61], are presented in Fig. 7F) and measured in this work for the STF-100 in the same conditions.

The fitting results reveal similarities for both Sr-deficient compounds. On the other hand, there are visible differences in comparison to the stoichiometric SrTi<sub>0.3</sub>Fe<sub>0.7</sub>O<sub>3-δ</sub>. Changes of the ohmic resistance in the function of pO<sub>2</sub> are negligible, because the CGO substrates are being practically insensitive for oxygen partial changes under the conditions used within this study [61]. The values for both STF-x compounds are comparable, taking into account the precision of 10% variation in the thickness of the electrolyte. As in our previous work, R<sub>gas</sub> strongly depends on the oxygen concentration and the slope of the double logarithmic plot (n = -1), suggesting that it is indeed a gas diffusion process. In the case of R<sub>1</sub> and C<sub>1</sub>, the value of pseudo capacitance



**Fig. 7** – Results of EIS measured at 700 °C and different oxygen partial pressures for STF-90 symmetrical cells (A) and corresponding DRT spectra (B), values of calculated contribution of series resistance (C), R1 (D) and  $R_{\text{gas}}$  (E) and relayed pseudo capacitances (F) as a function of oxygen partial pressure for STF70-90 and STF70-95.

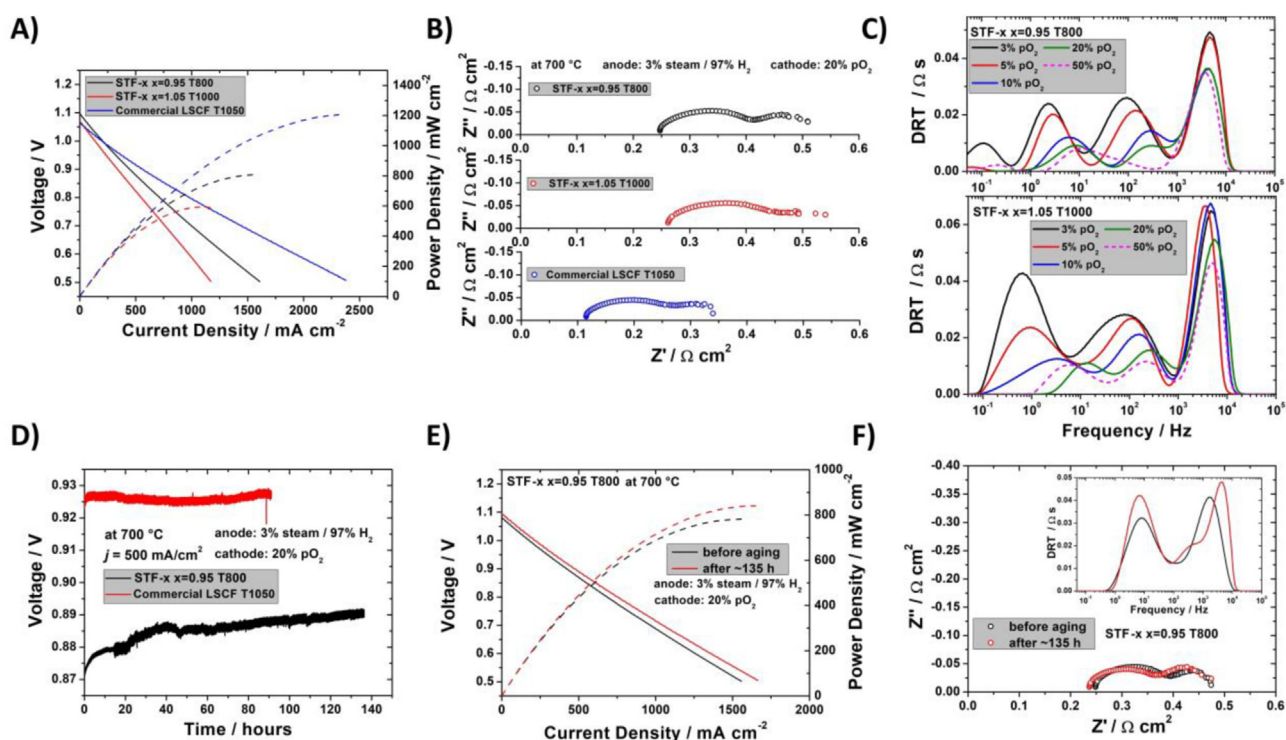
revealed a one order of magnitude increase in relation to the STF-100. The Sr-deficient materials show pseudo capacitance in the range of  $\sim 0.1 \text{ F cm}^{-2}$ , whereas the stoichiometric STF70 showed a pseudo capacitance of  $\sim 0.01 \text{ F cm}^{-2}$ , which is probably connected to the formation of a dense interfacial layer at temperatures of 900 °C and above for the Sr-deficient electrode materials and its chemical capacitance due to the accumulation of electro-active oxygen species (oxygen vacancies) in the “bulk” of the thin film structure [91]. This dense layer modifies the ORR/OER process at the interface between the ionic conductor (CGO) and MIEC electrode (STF70).

#### Solid oxide fuel cell test

The influence of strontium non-stoichiometry on the performance of solid oxide fuel cells at 700 °C was also checked. For the tests, Sr-deficient STF-95 sintered at 800 °C and Sr-enriched STF-105 sintered at 1000 °C were selected. The higher sintering temperature of STF-105 was chosen due to the lower sinterability of this compound. The reference cell with an LSCF cathode was sintered at 1050 °C. Fig. 8 A)–B) shows the current-voltage characteristics (I–V) and EIS for the tested fuel cells. For comparison, the I–V and EIS characteristics for the STF-100 are presented at Figure S.10. The maximum power density for fuels with STF-95, STF-105 and LSCF cathodes were, respectively: 809  $\text{mW cm}^{-2}$ , 594  $\text{mW cm}^{-2}$ , and 1206  $\text{mW cm}^{-2}$ . Although the EIS measurements revealed that all of the materials have different value of polarisation resistance (STF-95 – 276  $\text{m}\Omega \text{ cm}^2$ , STF-105 – 337  $\text{m}\Omega \text{ cm}^2$ , and LSCF – 237  $\text{m}\Omega \text{ cm}^2$ ), the electrochemical processes at 700 °C (syn. air and wet  $\text{H}_2$ ) are probably the same, as studied by DRT (presented in Figure S.11 A)). Differences are observed also for the ohmic resistances.

The lowest  $R_s$  was measured for the LSCF (115  $\text{m}\Omega \text{ cm}^2$ ), followed by the STF-95 (247  $\text{m}\Omega \text{ cm}^2$ ), and the STF-105 (261  $\text{m}\Omega \text{ cm}^2$ ). The increased ohmic resistance originates from the STF materials, which have much lower electronic conductivity than LSCF. Thus, the inferior performance of the cells with STF in comparison to the cells with LSCF is determined by the ohmic resistance. Interestingly, considering only STF-x materials the difference for ASR of symmetrical samples between STF-95 (sintered at 800 °C) and STF-105 (sintered at 1000 °C) was  $\sim 29.8\%$  (94  $\text{m}\Omega \text{ cm}^2$  and 122  $\text{m}\Omega \text{ cm}^2$  respectively). In SOFC applications difference of polarisation resistances decrease up to  $\sim 22.1\%$ . In the case of ohmic resistance, symmetric samples showed identical value 1.1  $\Omega \text{ cm}^2$  but in SOFC it slightly change ( $\sim 5.7\%$ ) in favor of STF-95. Which explains the better performance of cells with STF-95 material than with STF-105.

For a more detailed investigation of the influence of Sr non-stoichiometry on electrochemical processes of STF-x materials in fuel cells, EIS measurements as a function of  $p\text{O}_2$  were carried out. The results of the DRT analysis corresponding to the EIS data at different  $p\text{O}_2$  (Figure S.11 B)–C)) are presented in Fig. 8 C). Three main peaks can be observed. The low-frequency peak ( $\sim 1 \text{ Hz}$ ) is probably related to gas diffusion on the cathode and anode side. This low frequency peak looks similar for both cells at 20% and 50% of oxygen partial pressure, but the fuel cell with the STF-105 cathode seems be more sensitive to lowering the  $p\text{O}_2$ . In contrast, the middle frequency peak ( $\sim 100 \text{ Hz}$ ) at low  $p\text{O}_2$  (3%  $p\text{O}_2$ ) is comparable for both cells and with the increasing oxygen partial pressure, the fuel cell with the STF-95 cathode decreased more (practically disappearing at 50% of  $p\text{O}_2$ ). This frequency is often attributed to oxygen incorporation and diffusion (e.g. typical Gerischer element). This result is in line with the higher  $k^*$  value for strontium-deficient materials. For the high frequency peak



**Fig. 8** – I–V characteristic of anode-supported cells (A), Nyquist plots of impedance data measured at OCV (B), DRT analysis of EIS measured as a function of  $pO_2$  for cells with the STF-x cathodes (C), cell stability test under  $0.5 \text{ A cm}^{-2}$  current load (D) I–V plot before and after ageing of the fuel cell with the STF-95 cathode (E) and corresponding EIS (F).

(~5000 Hz), an observable small decrease of the peak for 20% and 50% of  $pO_2$  in contrast to the rest of the tested conditions can be noticed. Even though the high frequency peak is larger for the cell with the STF-105 cathode, the trend for both cells is comparable, and this peak is probably connected with ion transfer across the cathode/electrolyte.

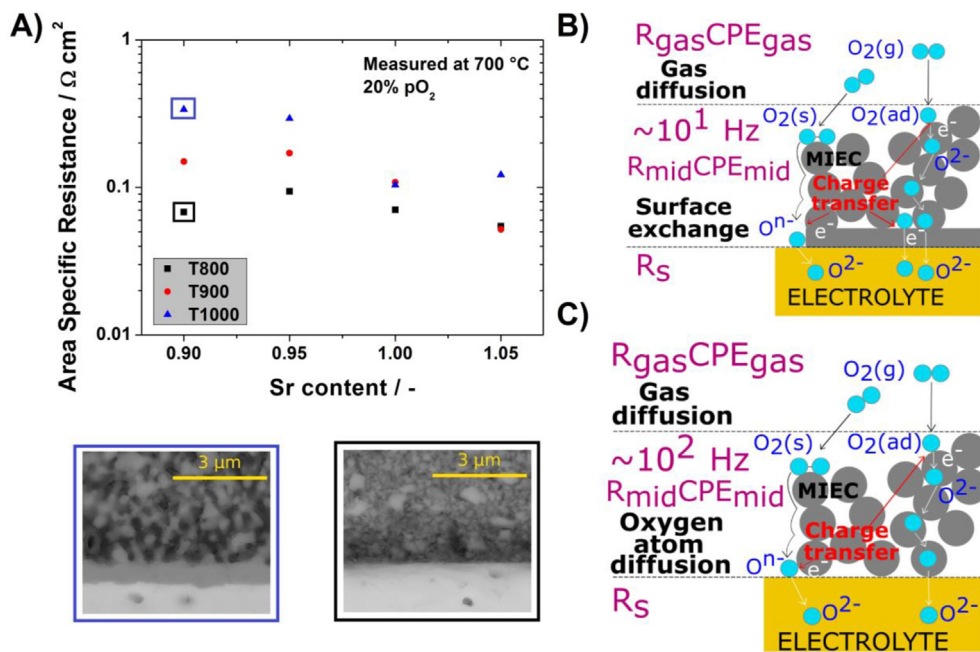
The performance of the STF-95 and the reference LSCF cathode was evaluated by monitoring the cell voltage output under a constant current load of  $0.5 \text{ A cm}^{-2}$  (Fig. 8 D) as a function of time. The initial voltages were  $\sim 0.87 \text{ V}$  and  $\sim 0.93 \text{ V}$  for the cell with the STF-95 and LSCF cathodes, respectively. During the 136-h the test, the voltage of the cell with the STF-95 cathode steadily increased by  $0.02 \text{ V}$  and it seems that it did not reach its maximum. In the case of the cell with the LSCF cathode, the voltage was almost stable over the 90 h of the test. The I–V and EIS measurements before and after the ageing test of the cell with the STF-95 cathode revealed improvement of the maximum power density and ohmic resistance with a concurrent small increase of ASR (Fig. 8 E–F)). Based on the SEM images taken before and after the stability test (Fig. S. 12), there are visible small difference of microstructure between two materials. STF-95 sintered at  $800 \text{ }^\circ\text{C}$  present smaller grains than LSCF sintered at  $1050 \text{ }^\circ\text{C}$  what was to be expected. Interestingly, both materials did not show significant changes in grain size, and no layer formed at the interface. Although the electrical results indicate the advantage of LSCF, STF-95 has the potential to be further modified, for example by infiltration, which will most likely allow it to be taken into account as a potential electrode for SOFCs.

## Discussion

Modifications at the A-site sublattice of STF-x material lead to important modifications of the main material properties (e.g. TEC,  $k^*$ ,  $D^*$ , and  $\sigma$ ) which in turn leads to differences in ASR values (Fig. 9A)).

One interesting feature of such modification is that electrochemical performance of the porous Sr-deficient materials can be easily limited by a too-high sintering temperature and the formation of a dense interface layer (Fig. 9 A) blue frame). The thickness of the dense interface layers formed at the sintering temperature of  $900 \text{ }^\circ\text{C}$  for the STF-90 electrode was  $\sim 200 \text{ nm}$ , whereas for the STF-95 it was slightly thinner ( $\sim 150 \text{ nm}$ ). The formation of this dense layer has also been confirmed by Yang et al. [59]. In that case, the layer formed at higher temperatures, probably due to the use of larger particles.

The dense interfacial layer clearly shows a chemical capacitance that depends on the oxygen storage capacity. For example, the chemical capacitance of STF5, STF35 and STF50 thin films was studied by Jung and Tuller [92]. They found a strong dependence of the capacitance on the iron content. For the same thickness of thin films, the capacitance of STF50 was almost an order of magnitude higher than for STF35, for which a value of  $\sim 12 \text{ mF cm}^{-2}$  for a  $160 \text{ nm}$  thick layer was reported at  $650 \text{ }^\circ\text{C}$ . Considering the higher content of oxygen vacancies for a higher Fe composition (STF70 instead of STF50) and extra vacancies due to Sr-nonstoichiometry (for lower temperatures), the capacitance of the layer is in reasonable agreement



**Fig. 9** – ASR as a function of strontium content for different sintering temperatures and SEM pictures of selected materials indicating significant microstructure differences (A), proposed model for porous STF-x cathode (B) and STF-x with a dense layer (C).

with the literature-proposed model for a thin film electrode with surface exchange-limited performance [91,92].

For materials sintered at low temperature (800 °C), characterised by a porous microstructure, the limiting electrochemical step is the process occurring at the middle frequency, identified as the adsorbed oxygen atom surface diffusion followed by a charge transfer reaction and incorporation into the lattice (Fig. 9C) [61,93]. As presented in Fig. 6 D), the contribution of the middle frequency peaks for the STF-90 and STF-95 is larger than for the STF-100 and STF-105, which is in line with the presented changes of  $D^*$ . In the case of the STF-90 and STF-95 sintered at higher temperatures ( $\geq 900$  °C), where Sr-non-stoichiometry induced the formation of a thin interface layer, the limiting electrochemical process changed to a surface exchange/bulk diffusion-limited process due to the lower apparent surface area of the dense layer (Fig. 9 B)). Interestingly, the highest electrochemical performance, measured in the symmetrical cell test, was obtained for the STF-105 electrode, which has a high surface content of Sr confirmed by XPS. It seems that the extra porosity, caused by inferior sinterability, led to the lowest ASR.

The maximum power density of the tested solid oxide fuel cell with STF-95 and STF-105 cathodes with similar microstructures (without a dense layer) differ (809  $\text{mW cm}^{-2}$ , 594  $\text{mW cm}^{-2}$ ), which is in agreement with the results obtained for EIS (94  $\text{m}\Omega \text{ cm}^2$ , 122  $\text{m}\Omega \text{ cm}^2$ ) for the symmetrical cells. The cell with the STF-95 cathode, with higher  $k^*$ , showed increased performance in the intermediate frequency range (Fig. 8C). The results of the cell performance with the new Co-free oxygen electrode are encouraging. To even further improve the functional properties, it is of interest to increase the total electronic conductivity of the electrode, e.g. by mixing with different material or by infiltration by highly conductive phases.

## Summary

In this work, the complex nature of the influence of the Sr-non-stoichiometry on the structural, transport and electrocatalytic properties of the promising  $\text{Sr}_x\text{Ti}_{0.7}\text{Fe}_{0.3}\text{O}_{3-\delta}$ -based materials was investigated.

The results showed that modification of the chemical composition by the introduction of non-stoichiometry affects the lattice parameter, i.e. a decrease of the Sr content results in a unit cell parameter increase, which has been connected (via XPS) to the reduction of  $\text{Fe}^{4+}$  to  $\text{Fe}^{3+}$  by the charge compensation mechanism and the introduction of oxygen vacancies. Lowering of the concentration of A-site cations (bulk Sr content) lowers the Sr-surface segregation. Based on XPS results, the Sr content is inversely correlated with the  $\text{Fe}^{+3}/\text{Fe}^{+4}$  ratio. Sr-deficient powders contained a lower amount of  $\text{Fe}^{4+}$  available for thermal reduction at higher temperatures. This was further confirmed by the thermogravimetry (TG), dilatometry (DIL) and temperature programmed (TPx) methods, which revealed changes in weight loss on heating and a lower thermal expansion coefficient due to the lower amount of strontium. One of the issues reported with STF materials with high iron content is their relatively high thermal expansion coefficient. Tailoring the Sr-stoichiometry can limit the TEC from  $\sim 21$  to  $\sim 17$ , which is a marked improvement for practical applications at intermediate temperature. In accordance with the existing defect model of STF, the introduction of Sr-deficiency results in decreased electronic (p-type) conductivity [65].

The electrocatalytic performance of bulk materials, as determined by the ECR technique, showed a positive influence of the Sr-deficiency on chemical surface exchange

coefficient ( $k^*$ ), and a negative effect on the chemical diffusion coefficient of oxygen ( $D^*$ ). In the electrochemical evaluation of porous electrodes, a complex trend in materials behaviour was found. Electrodes sintered at 800 °C showed similar electrochemical processes, with at least two clearly separated processes. Due to the small particle size of the synthesised powders and increased sinterability of the Sr-deficient materials, a continuous interfacial layer is formed even at sintering temperatures of 900 °C and above. This layer negatively influenced the electrode performance. Interestingly, the best overall electrode performance ( $\sim 50 \text{ m}\Omega \text{ cm}^2$  at 700 °C, including the contribution of gas diffusion) was obtained for Sr-rich material (STF-105). Even though the electrical conductivity of this compound was inferior to the stoichiometric one and it showed high surface Sr segregation, its performance was clearly superior. This high performance was attributed to the decreased sinterability of these materials, which restricted grain growth and maintained a high surface area available for oxygen reduction and oxidation processes.

Based on these results, rational design of electrode materials through tailoring A-site non-stoichiometry of the perovskites, based on  $\text{Sr}_x\text{Ti}_{0.3}\text{Fe}_{0.7}\text{O}_{3-\delta}$  ( $x = 0.90; 0.95; 1.00; 1.05$ ) is possible, but the relation between the basic physicochemical properties of bulk materials and porous electrode materials is complex. Even the well-studied issue of Sr-surface segregation requires further investigation to fully elucidate its effects. Moreover, the solid oxide fuel cell test confirmed that Sr-deficient STF- $x$  materials could be a viable alternative for Co-containing state-of-the-art materials after improvement of the ohmic resistance by, e.g., impregnation.

### Availability of data and material

The data that support the findings of this study are openly available in The MOST Wiedzy Open Research Data Catalog at 10.34808/yhx3-f485, reference number [94].

### Authors' contributions

A.M.: Investigation; Data curation; Visualization; Writing - original draft.

S.M.: Conceptualization; Methodology; Writing - review & editing.

P.B.: Investigation; Data curation; Writing - original draft;

T.M.: Conceptualization; Methodology; Validation;

K.G.: Investigation; Data curation;

J.K.: Investigation; Data curation;

P.J.: Methodology; Resources; Writing - review & editing; Supervision; Funding acquisition.

### Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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### Appendix A. Supplementary data

Supplementary data to this article can be found online at <https://doi.org/10.1016/j.ijhydene.2023.05.323>.

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