

SENSORLESS LOW SPEED PMSM MOTOR CONTROL WITH COGGING TORQUE COMPENSATION

Jarosław Guziński
Wydział Elektrotechniki i Automatyki
Politechnika Gdańska
Gdańsk, Poland
jaroslaw.guzinski@pg.edu.pl

Marcin Morawiec
Wydział Elektrotechniki i Automatyki
Politechnika Gdańska
Gdańsk, Poland
marcin.morawiec@pg.edu.pl

Zbigniew Krzemiński
Wydział Elektrotechniki i Automatyki
Politechnika Gdańska
Gdańsk, Poland
zbigniew.krzeminski@pg.edu.pl

Krzysztof Luksza
Wydział Elektrotechniki i Automatyki
Politechnika Gdańska
Gdańsk, Poland
krzluksz@gmail.com

Patryk Strankowski
Wydział Elektrotechniki i Automatyki
Politechnika Gdańska
Gdańsk, Poland
patryk.strankowski@pg.edu.pl

Abdellah Kouzou
Faculty of Sciences and Technology,
Ziane Achour University of Djelfa,
Djelfa, Algiera
kouzouabdellah@yahoo.fr

Abstract—The paper presents sensorless control of a low-speed permanent magnet synchronous machine with use of modified state observer. An overview of the PMSM motor used in the research setup was presented. The problem of drive torque ripple, resulting mainly from the occurrence of a significant cogging torque, was discussed. A solution compensating the torque ripple of the PMSM motor was proposed. A start-up procedure of the speed control system, allowing to run the drive system without speed and position sensors, was prepared. The field-oriented control with PI controllers of stator currents in the dq axes was implemented. The equations of a new, simplified version of the Krzemiński observer were presented. The observer has simpler structure of the gains, thus it is less computationally-intensive and easier to tune. The experimental results confirming the correct operation of the drive system were shown.

Keywords—Permanent Magnet Synchronous Machine, PMSM, state observer, field oriented control, cogging torque.

I. INTRODUCTION

The Permanent Magnet Synchronous Motors (PMSM) are used in many industrial applications, especially those requiring high driving parameters, such as precise speed control and high operation dynamics [1], [2]. Most often these machines are used in direct drives, i.e. without mechanical gear usage, where a low-speed motor is connected directly to the load, and the rotational speed does not exceed several hundred rpm [10]. Low-speed drives allow increasing the efficiency of energy conversion by eliminating the mechanical transmission power losses. These drives are most often used in: numerically controlled machine tools, robotic drives, printing machines, bending machines, etc. as well traction vehicles [2].

Utilizing the drive capabilities of PMSM is possible thanks to the control maximizing torque to current ratio. A very widespread of such methods is Field Oriented-Control (FOC) [1]. This method requires knowledge of the rotor's angular position and rotational speed. It can be achieved with position sensors, as well as sensorless, e.g. using state observers [3], [4].

The Luenberger motor electromotive force (EMF) observer utilizes the relationship between the angular rotor position and the motor EMF. As the EMF is not measured

directly, it must be estimated using the input variables (measured phase currents and the reference motor voltage) and the mathematical model of the PMSM. This observer treats the motor EMF as the estimated parameters. The Luenberger observer has less tendency to oscillate in the low speed range and is less computationally intensive than the Kalman Filter method [8].

In a MFC (Model Following Control) structure, the main controller generates a control signal for the object and its adjustable model. The additional controller, fed by a difference signal between the object output and model output, generates an additional control signal, which is added into the object input. Hence, if a tracking error occurs, an additional control signal is generated, whose task is to decrease the tracking error rapidly, and the object must follow the model. The reference model attempts to track the motor operating point. For example, in case of a step change in the motor load, the motor begins to slow down, and the motor's reference model begins to slow down too, because of the load estimator, which influences the drive model. Thus, the impact of distortion is eliminated by internal controllers in the drive model. This structure performs well for a speed range of single rpm (excluding standstill). It uses a back EMF observer to estimate the rotor position, but does not estimate the speed. This is a big advantage because of possible irregularity of estimated back EMF in this speed range, which makes the speed calculation difficult or impossible [5].

The Kalman filter is an estimator which provides optimal filtering with continuous Gaussian noises in the state and measurement, and known covariances of these noises. If the rotor speed and position (as extended states) are included in the dynamic model of the PMSM, the extended Kalman filter (EKF) can be used to linearize the non-linear state model for each new state estimate as it becomes available. The EKF is often used in PMSM drives to estimate the speed and position [6] [7].

Another interesting concept for this application is the Krzemiński disturbance observer. The idea of this observer is to treat the speed as the estimated parameter, and the EMF as a disturbance, and that's why from this point of view it is called the disturbance observer. The observer was

successfully used in drive systems with a squirrel-cage or wound-rotor induction motors, as well as for synchronous machines with surface or internally mounted permanent magnets. The Krzeminski observer is able to achieve a high accuracy of variable estimation for a wide speed operating range [22].

For the practical aspects of the sensorless drive operation it should also be mentioned that in a low speed PMSM machine drive torque ripple is a serious problem. It is mostly caused by the interaction between the magnetic field of the permanent magnets and time-varying stator reluctance, [4] - [13]. The ripple may negatively affect the operation of field-oriented control and should be compensated in the control system, [13] - [16].

This paper presents a complete speed and position sensorless PMSM control system, with cogging torque compensation. The main contribution of this paper is the introduction of a simplified version of Krzeminski speed and position observer. The new version has fewer observer gains and is thus easier to tune. Initial experimental verification of the proposed PMSM drive was previously carried out in [9]. In this paper additional experiments were conducted, with a speed and position sensor (an incremental encoder) for reference.

II. PERMANENT MAGNET SYNCHRONOUS MOTOR AND THE RESEARCH SETUP

The drive system, evaluated in this article, uses a 500STK1M type brushless permanent magnet synchronous motor made by Alxion [18]. It is a low-speed machine with a large pair number of poles also known as torque motor. The motor is shown in Fig. 1 and Table 1 presents the machine's most important data.

Fig. 2, presents the EMF of the 500STK1M motor at 60 rpm. The presence of 5 and 7 harmonics is visible in the EMF waveform, however, the EMF deformation is small, because the $THD_{EMF}=3.3\%$, which should not have a significant effect on the electromagnetic torque generated.

The test set-up consists of two coupled 500STK1M machines. One machine, working as a motor, is the test object, the other, working as a generator, is used as the load. An MMB Drives type MMB0051M back-to-back frequency converter was used to supply the torque motor. The converter consists of two voltage inverters connected by dc link. A control system with FPGA and DSP processor was used. The FPGA unit is an Altera Cyclone II (type EP2C8F256, 8256 LEs, 182 I/O), while the DSP is an ADSP21363 (333 Mhz, 666 MIPS). The controller was designed the earlier laboratory projects for use in research as well for commercial setups. Its open-source code is prepared in C language. To generate the output voltage of the converter, pulse width modulation using the Space Vector Modulation (SVM) was utilized. The modulation period and sampling period of the control system are equal and set to 150 μ s. The converter control is connected to a PC via USB. The dedicated C++ application, launched on the PC, enabled to load the control program into the DSP, save and read the DSP program variables and to visualize their waveforms.

The experimental results, presented in the article, were expressed in arbitrary units relative to the motor nominal data given in Tab. 1.

TABLE I
DATA OF 500STK1M PMSM TORQUE MOTOR [18]

Parameter	Abbreviation	Value	Unit
Power	P_n	12.6	kW
Voltage	$V_n^{(max)}$	330	V
Current	I_n	37.3	A
Motor rotational speed	n_n	600	rpm
Driving torque	T_n	210	Nm
Number of poles	p	36	-
Number of stator slots	N_s	108	-
Moment of inertia	J	0.216	$kg \cdot m^2$
Stator resistance	R_s	0.206	Ω
Stator inductance	L_s	1	mH
EMF constant	K_E	3.69	$V/rads^{-1}$

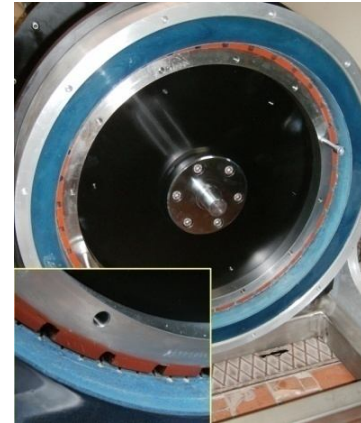


Fig. 1. An overview of the 500STK1M torque motor and a zoom-in on a couple of its magnetic poles

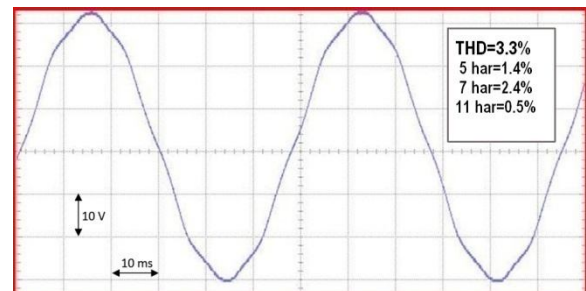


Fig. 2. The waveform of phase-to-phase electromotive force of 500STK1M torque motor at 60 rpm

III. COGGING TORQUE

In the case of PMSM motors there are two dominating torque ripple components [13]:

- cogging torque T_{cog} , resulting from the interaction between permanent magnets placed on the rotor and time-varying stator reluctance,
- electromagnetic ripple torque T_{elmag} resulting from a non-sinusoidal magnetic flux waveform.

The cogging torque component T_{cog} reaches up to several percent of the rated torque of the motor and is a function of the rotor position [10]:

$$T_{cog} = -\frac{l}{2} \psi_m^2 \frac{d\mathfrak{R}}{d\theta_r} \quad (1)$$

where: ψ_m is the magnetic flux of the permanent magnets, \mathfrak{R} is the total reluctance of the magnetic circuit, and θ_r is the angular position of the rotor.

To minimize the cogging torque of the 500STK1M motor, stator slots are made skewed which is common in similar drives [17]. Despite this, the amplitude of T_{cog} is large and has a significant impact on the torque motor operation.

The frequency of the cogging torque depends on the number of stator slots N_s and the number of poles of the rotor p . The period of the cogging torque ripple is defined by the following equation [11]:

$$\theta_{cog} = \frac{360^\circ}{LCM(N_s, p)} \quad (2)$$

According to the 500STK1 motor data from Table 1 the period of cogging torque ripple $\theta_{cog}=3.3^\circ$ because the least common multiple (LCM) of the number of stator slots and number of poles is $LCM(N_s, p) = 108$.

Sample waveforms of the estimated electromagnetic torque of 500STK1 motor are shown in Fig. 3. It can be seen in Fig. 3 waveforms that the significant torque pulsations appear in the torque waveforms. The shape of the torque pulsation is characteristic for the cogging torque. The frequency f_{cog} of these waveforms results from the mechanical frequency f_{mech} of the motor, the number of stator slots N_s and the number of pole pairs $2p$:

$$f_{cog} = f_{mech} \frac{N_s}{2p} \quad (3)$$

A significant cogging torque leads to the formation of velocity ripples and may cause incorrect operation of the PMSM drive [13] - [15]. This problem can be solved by e.g. using advanced speed controllers or the implementation of cogging torque compensation. The method of cogging torque compensation presented in the following paper is based on the estimation of the instantaneous motor torque and the determination of a proper compensating q current component (these calculations are performed in the *Tcog comp.* block in Fig.5). In the field-oriented control (described in part 5 of this paper), the reference q component of the stator current i_{sq}^{ref} can be determined based on the output signal of the speed regulator i_{sq}^{Rref} and the compensating component i_{sq}^{Cref} [14]:

$$i_{sq}^{ref} = i_{sq}^{Rref} + i_{sq}^{Cref} \quad (4)$$

The correct determination of the torque ripple compensating component i_q^{Cref} can be achieved using e.g. a fast current regulator [13], artificial neural network [2] or a torque estimator [16].

In the control system proposed in this paper, the current compensation component i_{sq}^{Cref} is determined in the torque compensation block according to the following equation:

$$i_{sq}^{Cref} = k_{cog} (T_e - T_{econst}) \quad (5)$$

where: T_e is the electromagnetic torque, T_{econst} is the constant component of the motor torque T_e , and k_{cog} is the torque compensation coefficient, which in this particular control system was chosen experimentally.

The value of the electromagnetic torque T_e was determined by the state observer.

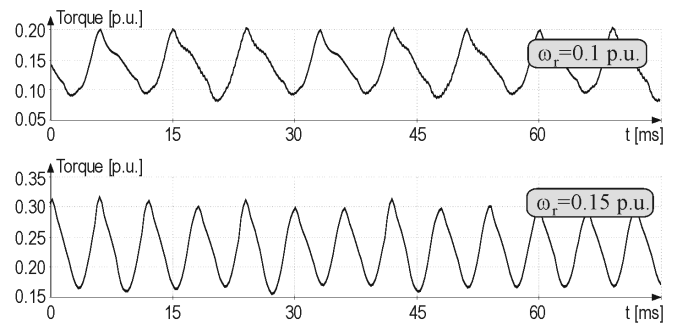


Fig. 3. The waveforms of the estimated torque of the 500STK1M motor at $\omega_r=0.1$ p.u. ($f_{cog}=108$ Hz) and $\omega_r=0.15$ p.u. ($f_{cog}=162$ Hz)

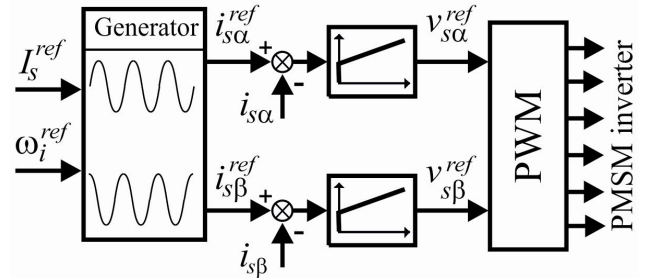


Fig. 4. The current control system of the PMSM torque motor used for the startup procedure

IV. STARTUP PROCEDURE OF THE DRIVE SYSTEM

Start up of the PMSM drive system operating without position and speed sensors requires an appropriate starting procedure [19], [20].

In the proposed solution, to allow the start-up of the PMSM motor, PI current controllers, operating in the fixed, orthogonal coordinate system $\alpha\beta$ (Fig. 4) were used. At the start of the system, sinusoidal reference current components $i_{s\alpha}^{ref}$, $i_{s\beta}^{ref}$ are applied, with the amplitude I_{sref} and angular frequency ω_i^{ref} gradually increasing, so as to force the motor to run at a low speed. Thanks to the current control, the inverter is protected against exceeding the allowed starting current.

After reaching the rotational speed of ca. 30 rpm, the state observer is switched on, which estimates all the parameters essential for the operation of the closed-loop control system. The next step is to switch the current controllers to work in the dq rotating coordinate system. In order to properly synchronize the position of the d-axis with the rotor position, the set-point value of the d-component of the stator current is set to $i_{sd}^{ref}=0$.

The next step of the start-up procedure is switching on the master speed regulator that sets the i_{sq}^{ref} current component, allowing to obtain the classic PMSM motor control structure discussed in section 5. The cogging torque is compensated in field-oriented control system by controlling of q-component current.

V. CONTROL STRUCTURE

The structure of the full control system is shown in Fig. 5. The drive system operates with field-oriented control. The magnetizing current is kept at $i_{sd}^{ref}=0$, which allows to achieve the minimal current and maximum torque [24]. The i_{sq}^{ref} current component is set by the speed controller with adding of the compensation of the cogging torque.

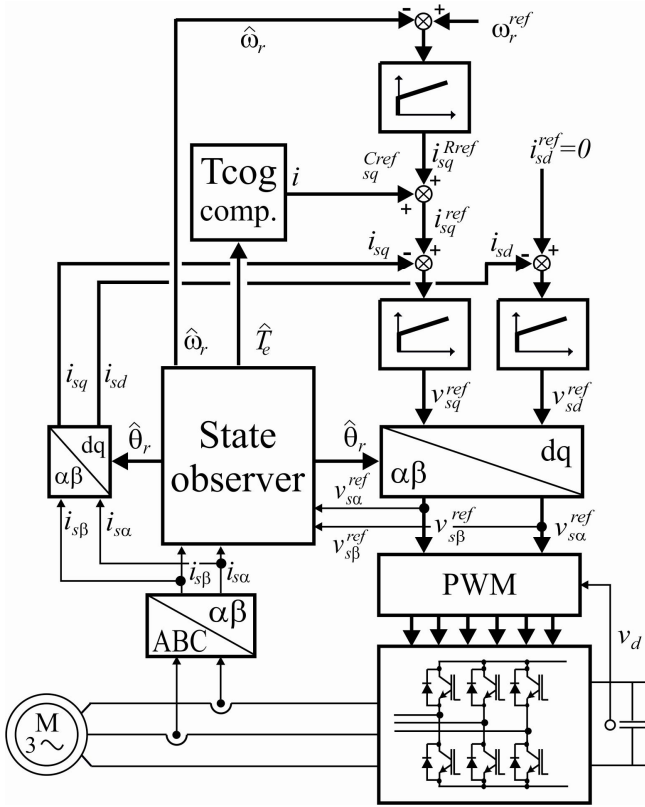


Fig. 5. Field oriented control system of the PMSM motor with cogging torque compensation

VI. THE OBSERVER OF ROTOR SPEED AND POSITION

The torque motor control requires the knowledge of the angular velocity and position of the rotor. These quantities can be measured using an encoder or resolver, or they can be estimated in the state variables observer [4].

The literature provides many solutions of observers that can be applied in the torque motor control system [21] - [22].

An interesting concept of the observer was proposed in [3], [22] and [23]. The PMSM version of this observer, in the previously known variants, has 7 gains and therefore requires considerable work with their selection. In the observer shown in [3] there is no correction block for the estimation of the rotor angular position. It was implemented in the observer version known from [23], however increasing the workload of calculations, extending the equations of the electromotive force model and introducing additional variables to stabilize the observer's operation.

In the torque motor drive system proposed in this paper, a simpler version of Krzeminski observer was used. The equations of the disturbance model were simplified and stabilizing variables were abandoned. The structure of the new version of the observer was selected and tested in a simulation program and then verified experimentally. The new version of the observer is less computationally-intensive and easier to tune, as it requires only three gains. The following observer equations were proposed:

$$\frac{d\hat{i}_{s\alpha}}{d\tau} = \frac{1}{L_s} (-R_s \hat{i}_{s\alpha} + \hat{\zeta}_\beta + u_{s\alpha}^{ref}) + k_1 (i_{s\alpha} - \hat{i}_{s\alpha}) \quad (6)$$

$$\frac{d\hat{i}_{s\beta}}{d\tau} = \frac{1}{L_s} (-R_s \hat{i}_{s\beta} - \hat{\zeta}_\alpha + u_{s\beta}^{ref}) + k_1 (i_{s\beta} - \hat{i}_{s\beta}) \quad (7)$$

$$\frac{d\hat{\psi}_{r\alpha}}{d\tau} = -\hat{\zeta}_\beta \quad (8)$$

$$\frac{d\hat{\psi}_{r\beta}}{d\tau} = \hat{\zeta}_\alpha \quad (9)$$

$$\frac{d\hat{\zeta}_\alpha}{d\tau} = -\hat{\omega}_r \hat{\zeta}_\beta - k_2 (i_{s\beta} - \hat{i}_{s\beta}) \quad (10)$$

$$\frac{d\hat{\zeta}_\beta}{d\tau} = \hat{\omega}_r \hat{\zeta}_\alpha + k_2 (i_{s\alpha} - \hat{i}_{s\alpha}) \quad (11)$$

$$\frac{d\hat{\theta}_r}{d\tau} = \hat{\omega}_r + k_3 \hat{\psi}_{rq} \quad (12)$$

$$\frac{d\hat{\omega}_{rF}}{d\tau} = k_F (\hat{\omega}_r - \hat{\omega}_{rF}) \quad (13)$$

$$\hat{\omega}_r = \frac{\hat{\psi}_{r\alpha} \hat{\zeta}_\alpha + \hat{\psi}_{r\beta} \hat{\zeta}_\beta}{\hat{\psi}_r^2} \quad (14)$$

In the observer described by (6)-(14) the angular rotor position θ_r and the angular velocity ω_r are estimated. The electromotive forces are calculated as follows:

$$\hat{e}_{s\alpha} = \psi_m \hat{\omega}_{rF} \sin(\hat{\theta}_r) \quad (15)$$

$$\hat{e}_{s\beta} = -\psi_m \hat{\omega}_{rF} \cos(\hat{\theta}_r) \quad (16)$$

where the electromotive torque is using the following equation:

$$\hat{T}_e = \frac{\hat{e}_{s\alpha} \hat{i}_{s\alpha} + \hat{e}_{s\beta} \hat{i}_{s\beta}}{\hat{\omega}_{rF}} \quad (17)$$

The structure of the variable estimation system was presented in Fig. 6. The estimated q component of the rotor magnetic flux is used in (12), where the angular position of the rotor is calculated. It allows correcting the error value of the estimated angular position of the dq coordinate system.

An incremental encoder was added to the research setup in order to obtain a measured speed for data acquisition purposes only. It allowed calculating the observer's error and verifying its accuracy. A variable resistor was also used to load PMSM generator.

VII. EXPERIMENTAL RESULTS

Experimental tests confirmed the correct operation of the presented sensorless control system with torque ripple compensation.

Without a torque compensation system, the drive did not run steadily above the speed of about 0.25 p.u., due to significant current ripple activating the inverter's over current protection.

The effect of the torque compensation is presented in Fig.7. As can be observed, the torque ripple has been reduced by about 70%.

The reduction of the torque vibration allowed the correct operation of the speed control system. Figure 8 shows the waveforms of rotor speed (estimated by the observer and measured by the encoder) and i_{sq} current for a motor speed increase (a ramp function) to about 0.6 p.u. Such a speed range was impossible to achieve without the operation of the torque ripple compensation system.

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